



**ATTACHMENT 2**

**PROPOSED STORMWATER MANAGEMENT  
FACILITY**



January 25, 2018  
MTE File No.: C33886-100

Mr. Lou Freymond  
Freymond Lumber Ltd.  
2287 Bay Lake Road, RR1  
Bancroft, ON K0L 1C0

Dear Mr. Freymond:

**Re: Freymond Quarry  
Proposed Stormwater Management Facility**

## 1.0 INTRODUCTION

The purpose of this memorandum is to address the potential impacts associated with discharging water from the proposed Freymond Quarry, located on part of Lots 51 & 52, Concession W.H.R., Township of Faraday, Concessions of Hastings, or 2287 Bay Lake Road, Bancroft, Ontario (hereafter referred to as the "Site").

The quarry lands are proposed to drain by gravity to a stormwater management pond located in the southeast corner of the Site, which is proposed to provide the required water quality and quantity control before discharging to an unnamed stream south of the Site (hereafter referred to as the "South Stream"), which flows east to the York River approximately 500 m downstream.

## 2.0 STORMWATER MANAGEMENT CRITERIA

The proposed stormwater management works shall be designed in accordance with the Ministry of Natural Resources and Forestry (MNRF) and the Ministry of the Environment and Climate Change (MOECC) *Stormwater Management Planning and Design Manual* (MOE, 2003). As the stormwater management facility is proposed to outlet to a stream system, water quality and erosion controls must be incorporated. Additionally, the stream crosses several access routes for the area, including Highway 62 going into the Town of Bancroft, so the stormwater management plan must include water quantity control to mitigate any potential flood hazard. The criteria for development of this stormwater management plan are therefore as follows:

- Provide an *Enhanced* (MOE, 2003) level of quality control,
- Provide 24 hour detention of the 25 mm 4-hour Chicago storm event for erosion control,
- Provide pre- to post-excavation peak flow matching for the 2 through 100-year return period storm events.

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### 3.0 WATER QUALITY

The Ministry of Natural Resources and Forestry has specified that stormwater management facilities which outlet to the South Stream must provide an *Enhanced* level of quality control as described in Table 3.2 of the MOECC *Stormwater Management Planning and Design Manual* (MOE, 2003).

The Site is proposed to be excavated in 4 phases from the initial excavated condition to the final rehabilitated condition. The layout of the excavation, overburden stockpiling, existing and remediated vegetation, and stormwater management facility on the Site was provided in sketches to MTE from MHBC. The sketched areas were then quantified by MTE for design purposes. Both the initial and quantified sketches, as well as a table summarizing the hydrologic properties of each area, are included in the appendices. It was assumed that both the excavation and the overburden stockpiling areas would be completely impervious for this design; as there is very little overburden on-site to stockpile. As such, the potential exists for these areas to be completely exposed bedrock. Phase 3 of the development has the largest amount of open excavation and therefore the highest impervious value. For these reasons, it will be considered the 'design phase' for the purpose of this stormwater management plan.

During the most intense phase of excavation (Phase 3), the Site has an imperviousness of approximately 55.5% over its 33.27 ha area. With these parameters, the design of a wet pond facility requires a permanent pool volume of 5,032 m<sup>3</sup> and an extended detention storage volume of 1,331 m<sup>3</sup>, the latter of which is to be retained for a minimum of 24 hours (MOE, 2003). The proposed stormwater management facility has a permanent pool volume of 7,680 m<sup>3</sup>, sufficient for the subject site. General facility details, including quality control, are outlined in **Table 1** below.

### 4.0 EROSION CONTROL

Erosion control will be provided as per the MOECC manual by ensuring that the volume of the 25 mm 4-hour Chicago design storm event will be retained in the stormwater management facility for a minimum of 24 hours (MOE, 2003).

Design storm event modelling for the Site was performed using MIDUSS (version 2.25 revision 473) software and is included in the appendices. Rainfall Intensity-Duration-Frequency (IDF) data was obtained from the Ontario Ministry of Transportation (MTO) IDF curve lookup application for the Bancroft area, which was then used (in conjunction with the MIDUSS IDF curve fit tool) to create Chicago design storm parameters for the 2 through 100-year return period events. Chicago design storm parameters for the 25 mm event is based on the 2-year return period with a lowered "A" coefficient to obtain the desired 25 mm total rainfall depth. The total volume of the 25 mm event during the design extraction phase is 4,392 m<sup>3</sup>. Information on the IDF parameters is included in the appendices.

## 5.0 WATER QUANTITY

In order to mitigate downstream flooding considerations, post-excavation peak flows into the South Stream will be controlled to pre-excavation levels for the 2 through 100-year return period events. As previously discussed, Chicago design storm parameters were derived using the MTO IDF curve lookup application for the Bancroft area. Information on the pre-excavation catchment area draining to the South Stream (catchment 104, as detailed in **Figure 14: Drainage Assessment – Existing Conditions**) is included in the appendices, along with catchment parameters for each of the excavation phases. The pre- and post-excavation MIDUSS modelling is also included in the appendices; the results of which are summarized in **Table 2** below.

Though the Site is proposed to be remediated after the extraction is complete, there will always be an increased drainage area directed to the South Stream (catchment 504 as illustrated on **Figure 18: Drainage Assessment – Phase 4**). As such, the stormwater management pond is proposed to remain in the remediated condition to continue to provide peak flow attenuation and erosion control to the South Stream. Additional flow due to groundwater seepage from the excavation is assumed to be negligible.

## 6.0 STORMWATER MANAGEMENT FACILITY DESIGN

### 6.1 Facility Outlet

As described in **Sections 3.0 & 4.0** above, both the 1,331 m<sup>3</sup> MOECC water quality volume and the 4,392 m<sup>3</sup> 25 mm storm event volume must be retained for a minimum of 24 hours. It is the smaller MOECC quality volume which limits the maximum size of the extended detention orifice. An orifice drawdown design sheet is included in the appendices and indicates that based on the pond geometry; a 100 mm diameter orifice may be used to provide minimum 24-hour extended detention for the aforementioned volumes. The extended detention outlet control is therefore proposed to be a 100 mm diameter orifice with its invert set at the permanent pool elevation of 332.00 m to ensure adequate fall exists to the South Stream. The peak extended detention ponding elevation occurs for the larger 25 mm event volume and is 332.68 m, as outlined in **Table 1**.

In order to provide quantity control for larger storm events as described in **Section 5.0**, a 1.25 m horizontal weir is proposed at an elevation of 332.70 m, which is above the extended detention storage levels. The peak ponding elevation and storage volume for each design storm are shown in **Table 2**.

The weir, along with the aforementioned orifice, is proposed to be located within a precast concrete box manhole as illustrated on **MTE Figure 19: Stormwater Management Facility**. The 1.25 m quantity control weir is to be located at the top of the weir wall, at an elevation of 332.70 m as specified on the drawing. The top of the precast box manhole outlet structure is to be open, covered by galvanized ditch inlet grating, and set at an elevation of 333.40 m. The purpose of the open top outlet structure is to provide an emergency overflow outlet above the maximum modelled ponding elevations.

**TABLE 1: Stormwater Management Facility Design Characteristics**

General	Facility Characteristics
Stormwater Management Facility Type	Wet Pond
Required MOECC Water Quality Protection	Level 1 (Enhanced)
Total Contributing Area	33.27 ha
Imperviousness	55.53%
Bottom Elevation (of main facility)	329.00 m
<b>Storage</b>	
Unit Area Storage Volume Requirements as per SWMMP (MOE 2003)	191.24 m <sup>3</sup> /ha
Required Total Volume	6,363 m <sup>3</sup>
<i>Permanent Pool</i>	
Required Permanent Pool Volume	5,032 m <sup>3</sup>
Provided Permanent Pool Volume	7,680 m <sup>3</sup>
Permanent Pool Elevation	332.00 m
<i>Extended Detention</i>	
Minimum Required Volume	25 mm Event
Approximate Drawdown Time (for MOECC Table 3.2 requirement)	71.0 hr
Extended Detention Elevation (for 25 mm event)	332.68 m
Peak Release Rate for Extended Detention (for 25 mm event)	0.017 m <sup>3</sup> /s
<b>Settling</b>	
Required Settling Length	77 m
Provided Settling Length	90 m
<b>Outlet Controls</b>	
<i>Precast Concrete Box Manhole Outlet Structure</i>	
Orifice 1 Diameter (Extended Detention)	100 mm
Orifice 1 Invert Elevation (Extended Detention)	332.00m
Weir 1 Crest (Quantity Control)	1.25 m
Weir 1 Side Slopes (Quantity Control)	Vertical
Weir 1 Elevation (Quantity Control)	332.70 m

**TABLE 2: MIDUSS Modelling Summary**

Storm Event	Pre-Excavation Peak Flow (m <sup>3</sup> /s)	Pre-Excavation Runoff Volume (m <sup>3</sup> )	Post-Excavation Pond Inflow (m <sup>3</sup> /s)	Post-Excavation Runoff Volume (m <sup>3</sup> )	Post-Excavation Pond Outflow (m <sup>3</sup> /s)	Required Storage Volume (m <sup>3</sup> )	Peak Ponding Elevation (m)
25 mm	0.098	1333	2.709	4392	0.017	4062	332.68
2 Year	0.169	1765	3.414	5220	0.064	4682	332.78
5 Year	0.421	3260	4.829	7758	0.288	5961	332.97
10 Year	0.653	4385	5.738	9494	0.443	6617	333.06
25 Year	0.982	5972	6.759	11787	0.680	7494	333.19
50 Year	1.314	7124	7.603	13370	0.873	8138	333.28
100 Year	1.639	8438	8.477	15110	1.098	8845	333.38

The box manhole will outlet directly to a 900 mm diameter Smooth Wall Boss HDPE pipe at a minimum 0.5% slope; sufficient to convey the peak facility outflow of 1.098 m<sup>3</sup>/s to the South Stream. Approximately, 87.1 m of pipe will be installed until its spring line emerges from the embankment to the South Stream, at which point the pipe will be terminated and a rip-rap lined energy dissipation pad shall be graded into the embankment to reduce the effects of erosion. Refer to **MTE Figure 19: Stormwater Management Facility** for more details.

## 6.2 Settling Length

Since the majority of annual rainfall occurs in storms less than or equal to the 25 mm storm event, the majority of water borne sediment is also transported to the stormwater management facilities in these less intense events<sup>1</sup>. Therefore, the facility has been designed using a berm with an elevation of 332.70 m to provide a long settling length for the 25 mm event and target these smaller flows, while allowing the upper portions of the facility to provide unimpeded storage and a greater area of flow for the more intense storm events.

The facility design is based on classic particle settling and flow dispersion equations as presented in the MOECC *Stormwater Management Practices Planning and Design Manual* (MOE, 1994). The design flow for the settling length was taken to be the peak outflow from the facility during the 25 mm event. Furthermore, the settling velocity was assumed to be 0.00001300 m/s in order to ensure the settling of particles >20 µm (MOE, 1994). Additionally, flow dispersion and scour velocity checks were made, including the permanent pool area, to ensure that sufficient length is provided to mitigate all concerns. The required settling length was calculated to be 77 m, whereas approximately 90 m of settling length is provided in the pond. Settling calculations are included in the appendices.

## 6.3 Additional Features

The following additional features have been incorporated into the stormwater management facility design:

- The permanent pool will be excavated to 3 m where possible to provide additional settling volume and reduce cleanout frequency;
- The maximum active storage retention depth has been limited to 1.5 m;
- For safety, side slopes have been limited to 4:1 for 3 m below the permanent pool, and 3:1 for 1.5 m above the permanent pool;
- A minimum 3 m wide and 0.3 m deep flat shelf is proposed around the perimeter of the permanent pool elevation to serve as a wetland planting area;
- An access & maintenance road of 4 m width has been incorporated into the design to ensure sufficient access to the outlet structures and pond bottom for ease of inspection and maintenance. The access road will have a maximum longitudinal slope of 10:1 and a minimum inside radius of curvature of 10 m; and,
- As this pond will be constructed below the groundwater level, an impermeable (geotextile or clay) pond liner may be required.

1. From MOE-1994, Figure C.1: 54% less than 5mm, 75% < 10mm, 93% < 15mm and 99% < 25mm

## 7.0 MONITORING PROGRAM

Effluent from the SWM facility shall be sampled monthly under non-freezing conditions, after significant rainfall events (>8 mm), provided that there are sufficient volumes of water to be sampled, for a period of two years after operations commence, as specified below:

- Samples are to be analyzed for the following parameters:
  - a) Total Suspended Solids (TSS).
  - b) Total Ammonia.
  - c) Total Petroleum Hydrocarbons (fractions F1 through F4).
- During sampling, the pH and temperature of the water sample will be collected and recorded in-situ. The concentration of un-ionized ammonia shall be calculated using the total ammonia concentration, pH, and temperature using the methodology stipulated in "Ontario's Provincial Water Quality Objectives" dated July 1994, as amended, for ammonia (un-ionized).
- The quarry operator shall measure, record, and calculate the volume of flow discharging over the control structure on each day of sampling.
- After two years of operations, the effluent monitoring program shall be reviewed on an annual basis and revised if necessary.

## 8.0 CONCLUSIONS & RECOMMENDATIONS

Based on the foregoing analyses, it is concluded that:

- The described stormwater management facility will provide adequate quality and flood control measures for stormwater runoff from the Site to the South Stream; and,
- The described stormwater management facility will provide best management practices for erosion control based on MOECC guidelines.

These conclusions lead to the following recommendations:

- That a fluvial geomorphological assessment of the South Stream be performed in order to establish specific erosion control criteria;
- That the facility design be reviewed in conjunction with the updated *Environmental Impact Statement* when it becomes available, specifically with respect to any mitigation measures for the South Stream;
- That the stormwater management facility be constructed as described in this memo, including the specified outlet, settling length, and impermeable pond liner;
- That the extraction operator may not at any point exceed the total disturbed area and/or area of exposed bedrock face assumed for the design phase of the stormwater management facility, as described in **Section 3.0**;
- That the facility effluent be monitored as described in **Section 7.0** to verify facility performance; and,
- That the facility remain in the rehabilitated condition to continue to provide peak flow attenuation and erosion control for the South Stream.



Mr. Lou Freymond, Freymond Lumber Ltd.

January 25, 2018

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We trust the above and enclosed is in order, if you wish to discuss further, please do not hesitate to contact the undersigned.

Yours truly,

**MTE CONSULTANTS INC.**

Charles Carré, E.I.T.  
Designer

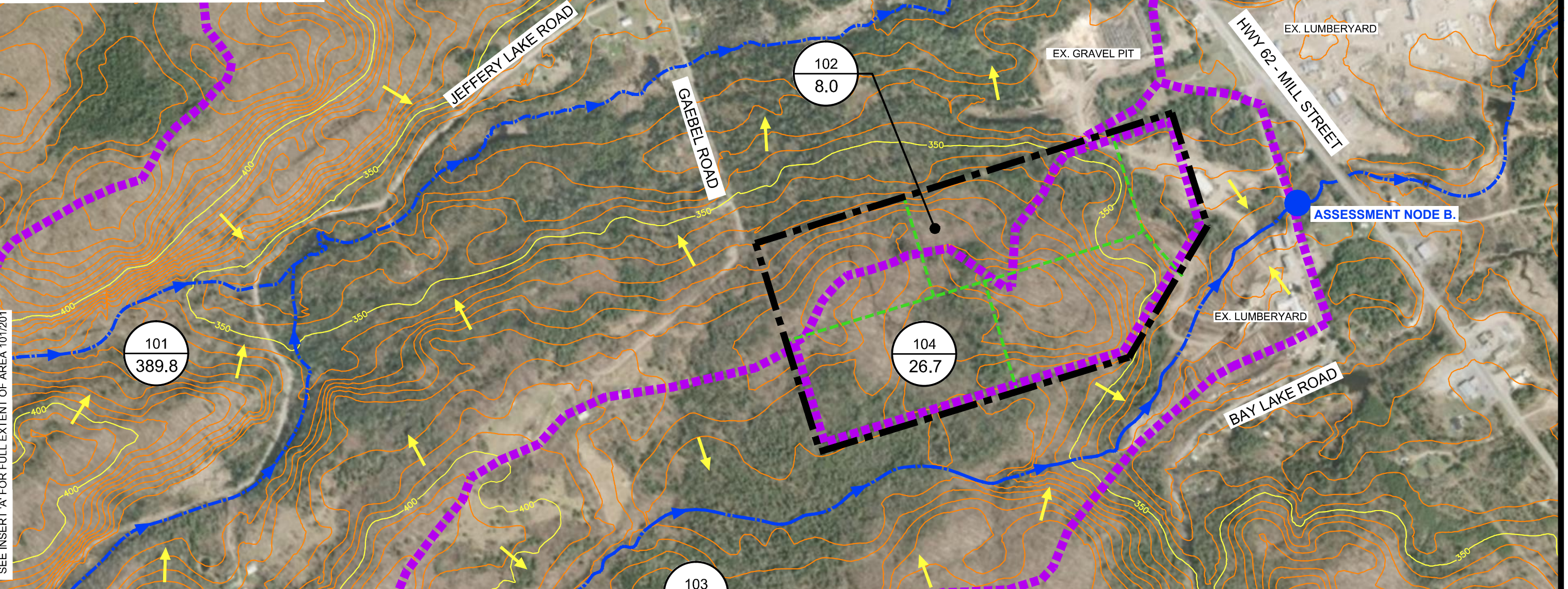
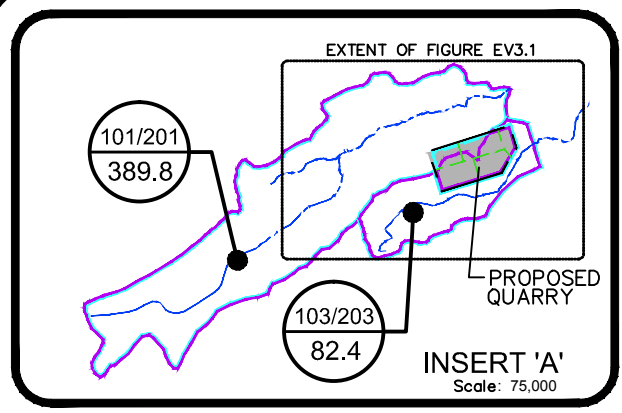
Jeff Martens, P. Eng.  
Design Engineer

cc: Mr. Jay Flanagan, MTE Consultants Inc.

Mr. Robin E. Craig, Environmental Consultant, Certified Wildlife Biologist



November 11, 2016 - 10:00 a.m. - Plotted By: kmadsen  
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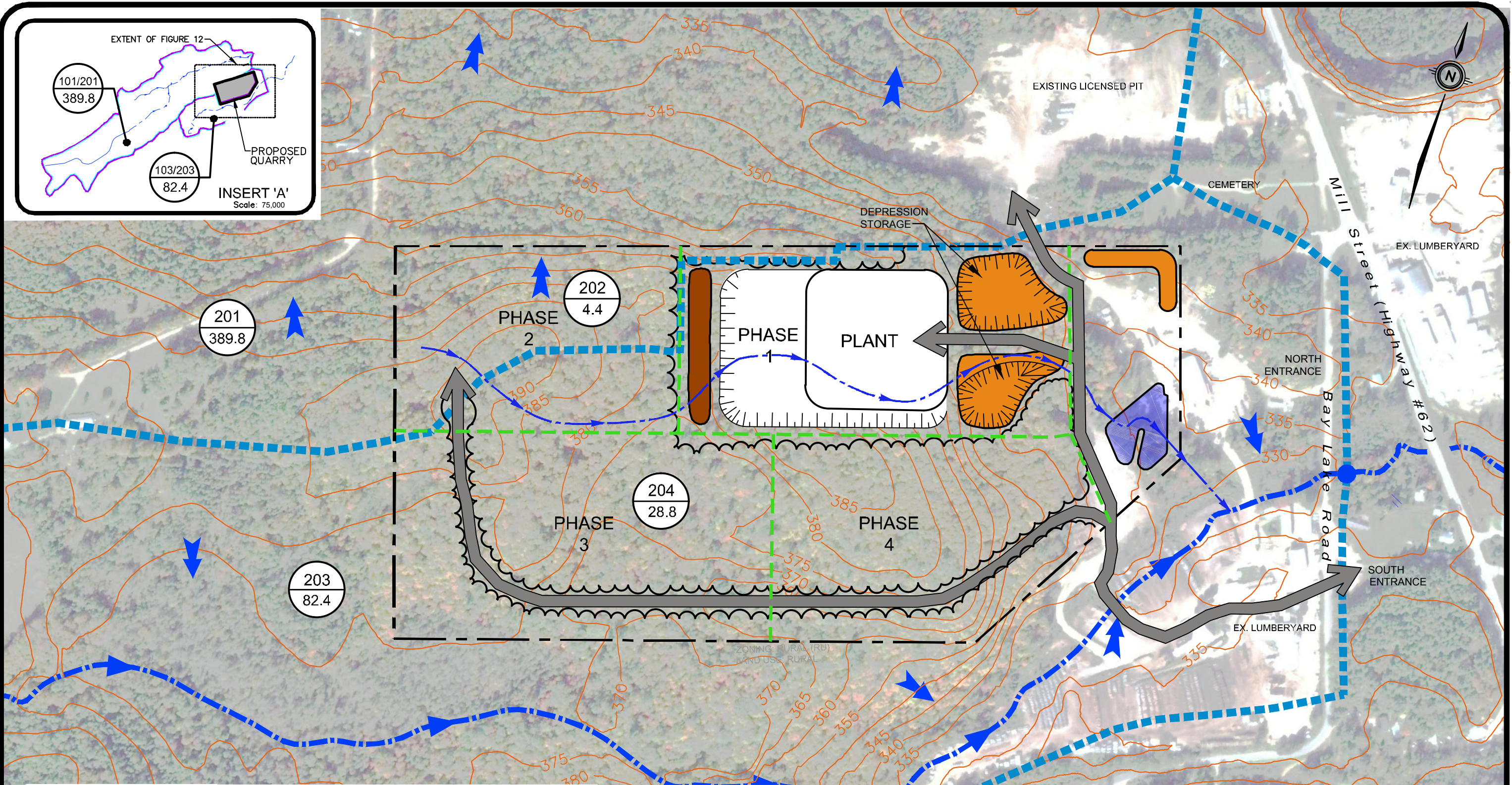
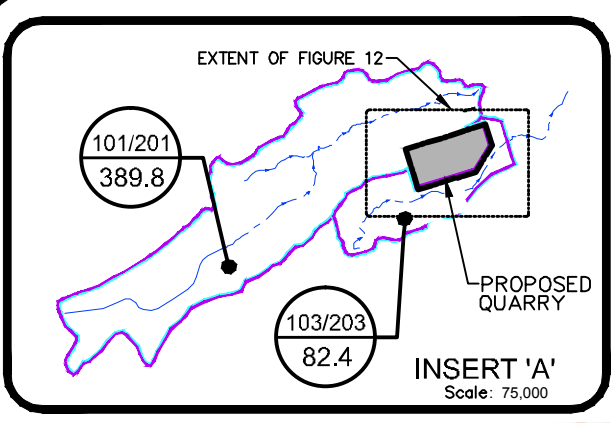
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- EXISTING SURFACE CONTOURS (5m)
- CATCHMENT ID# (PRE=100'S)
- CATCHMENT AREA (ha)
- ASSESSMENT NODE
- EXISTING SURFACE CONTOURS (50m)
- DIRECTION OF OVERLAND FLOW
- EXISTING CREEK
- PHASE BOUNDARY

**DRAINAGE ASSESSMENT: EXISTING CONDITIONS**

*Project Name*  
**Freymond Proposed Quarry**

<i>Site</i> Bancroft, Ontario		<i>Client</i> Freymond Lumber Limited	
<i>Scale (11x17)</i> 1:7,500	<i>MTE Project No.</i> 33886-100	<i>Date</i> November 2016	<i>Figure No.</i> <b>14</b>



**LEGEND**

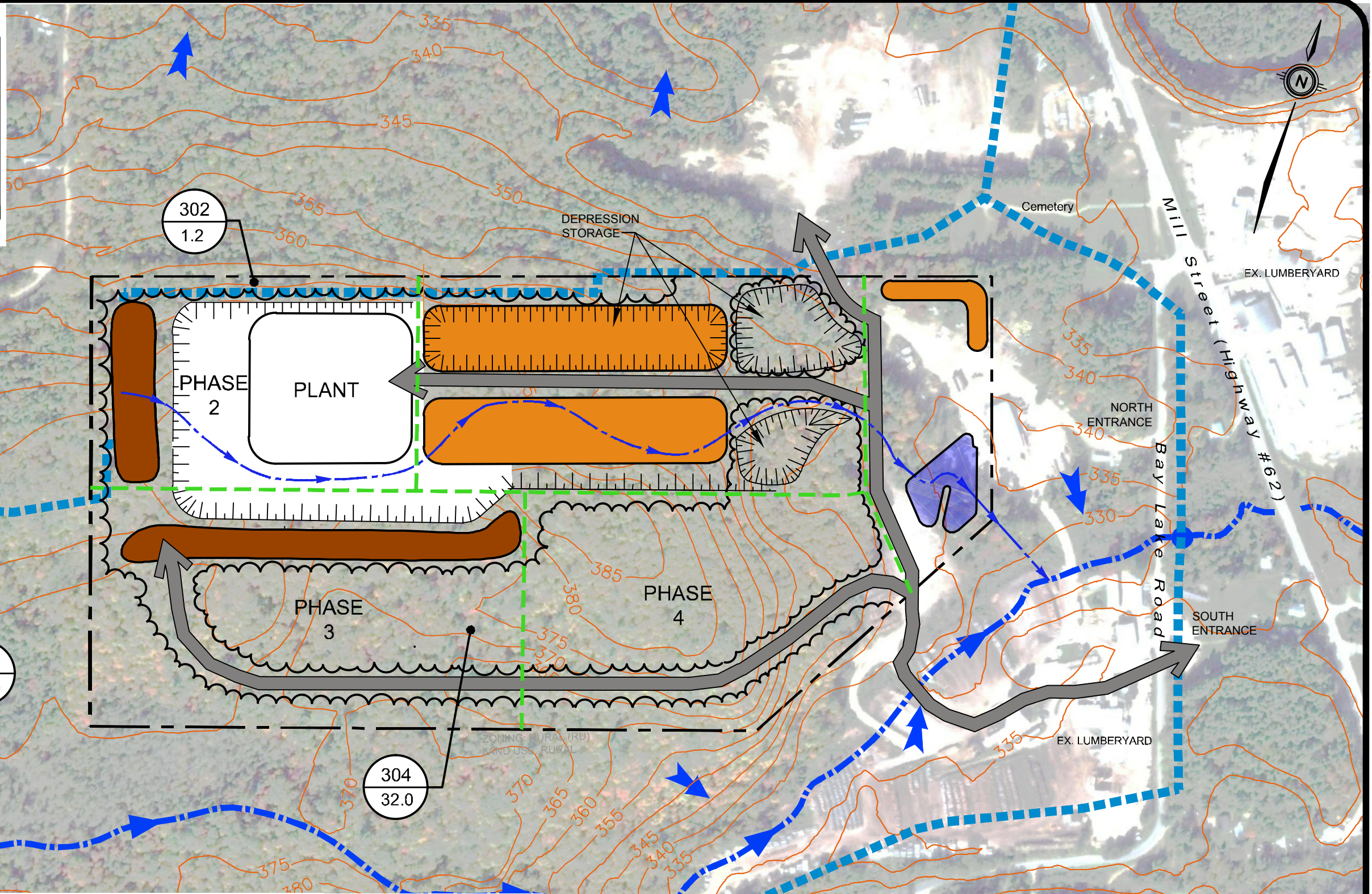
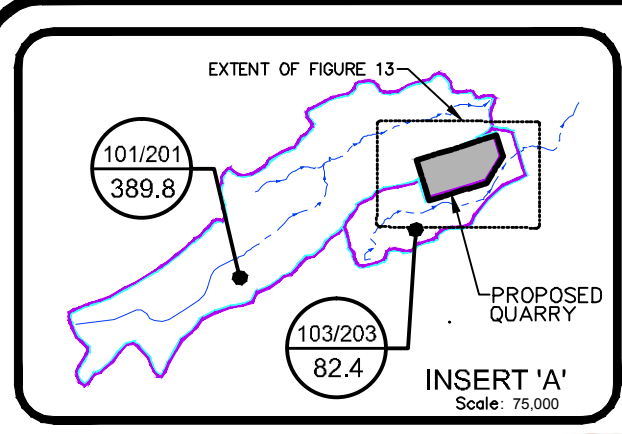
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	PHASE BOUNDARY		DIRECTION OF OVERLAND FLOW		PLANT
	CATCHMENT ID#		EXISTING CREEK		STORMWATER MANAGEMENT POND
	CATCHMENT AREA (ha)		OVERBURDEN		

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### DRAINAGE ASSESSMENT: PHASE 1

Project Name  
**Freymond Proposed Quarry**

Site Bancroft, Ontario	Client Freymond Lumber Limited
Scale (11x17) 1:4000	MTE Project No. 33886-100
Date November 2016	Figure No. <b>15</b>

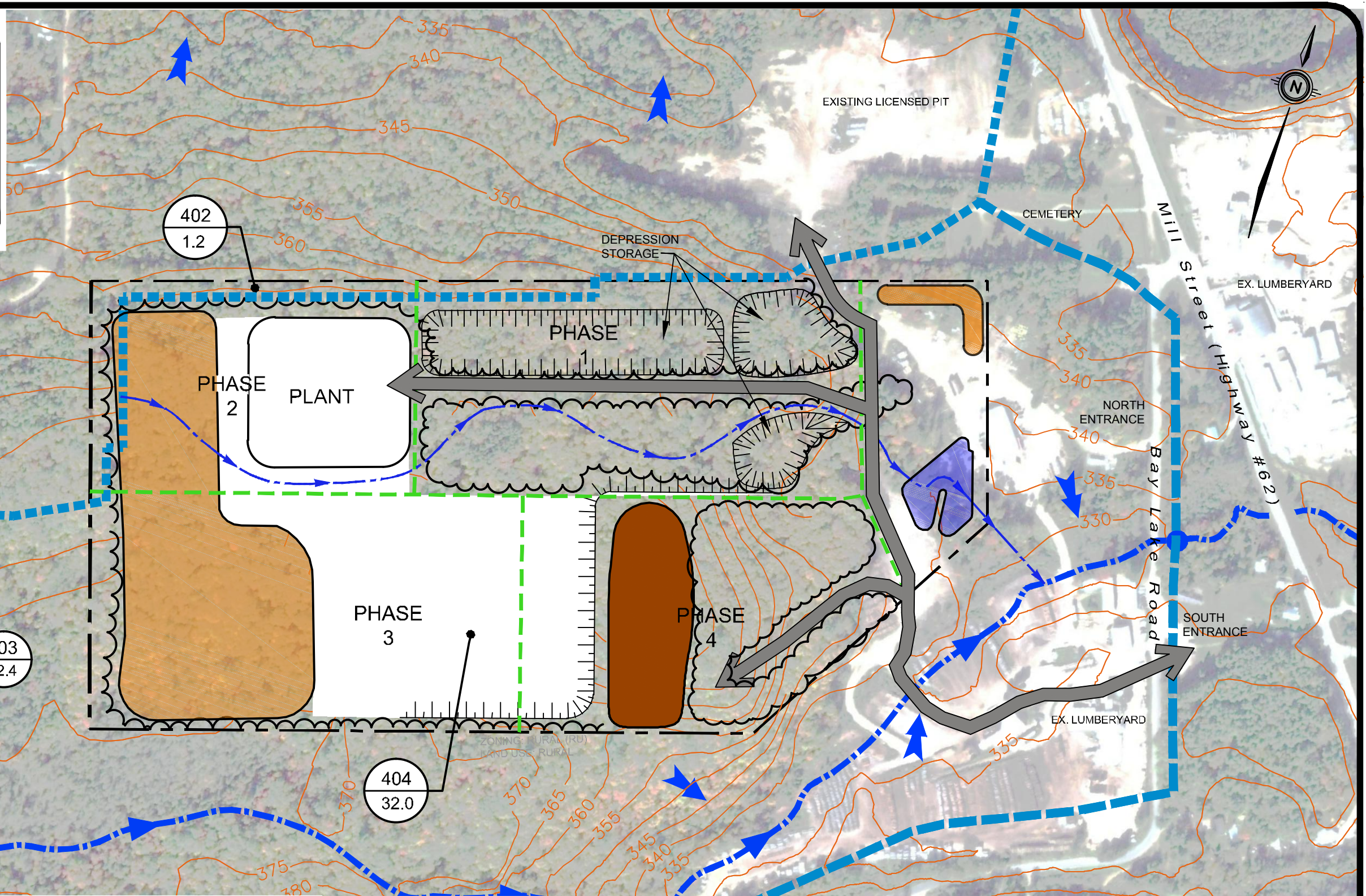
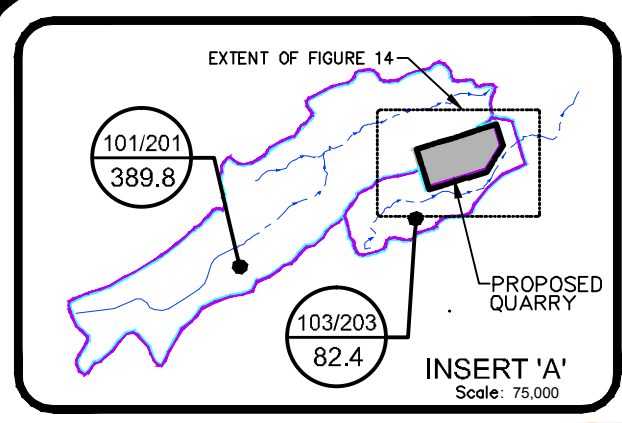


**LEGEND**

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	PHASE BOUNDARY		DIRECTION OF OVERLAND FLOW		PLANT
	CATCHMENT ID#		EXISTING CREEK		STORMWATER MANAGEMENT POND
	CATCHMENT AREA (ha)				OVERBURDEN

**DRAINAGE ASSESSMENT: PHASE 2**

Project Name <b>Freymond Proposed Quarry</b>			
Site Bancroft, Ontario		Client Freymond Lumber Limited	
Scale (11x17) 1:4000	MTE Project No. 33886-100	Date November 2016	Figure No. <b>16</b>



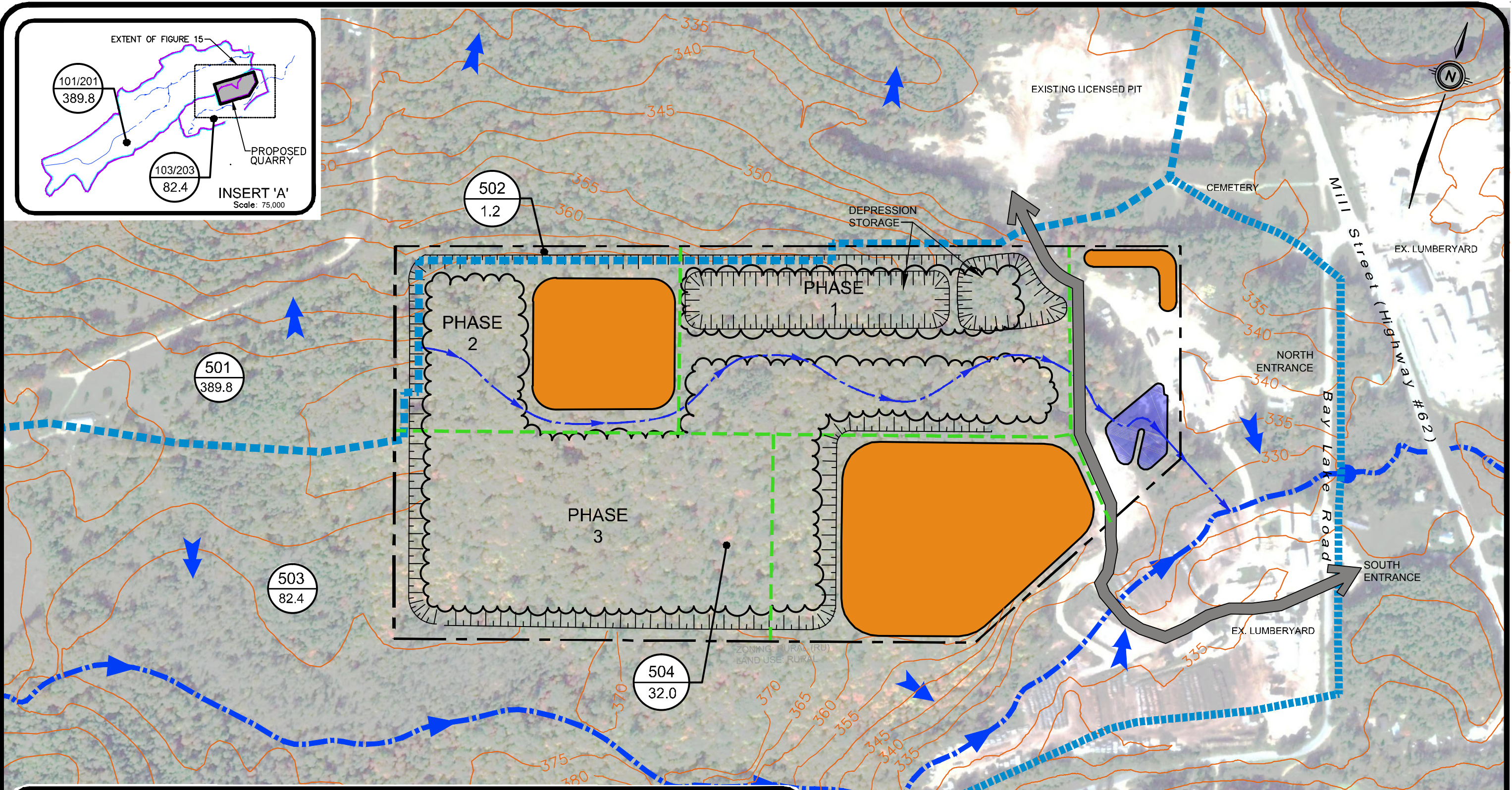
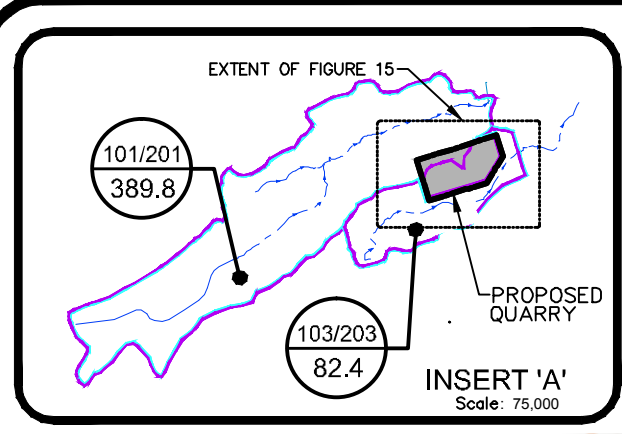
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	PHASE BOUNDARY		DIRECTION OF OVERLAND FLOW		PLANT
	CATCHMENT ID# CATCHMENT AREA (ha)		EXISTING CREEK		STORMWATER MANAGEMENT POND
					OVERBURDEN

**DRAINAGE ASSESSMENT: PHASE 3**

Project Name <b>Freymond Proposed Quarry</b>			
Site Bancroft, Ontario		Client Freymond Lumber Limited	
Scale (11x17) 1:4000	MTE Project No. 33886-100	Date November 2016	Figure No. <b>17</b>

**MTE**  
Engineers | Scientists | Surveyors



**LEGEND**

- PROPOSED FREYMOND QUARRY (THE "SITE")
- EXTRACTION CATCHMENT AREA
- PHASE BOUNDARY
- CATCHMENT ID#
- CATCHMENT AREA (ha)
- ASSESSMENT NODE
- EXISTING SURFACE CONTOURS (5m)
- DIRECTION OF OVERLAND FLOW
- EXISTING CREEK
- EXISTING VEGETATION OR NEW VEGETATION
- AREA BEING REHABILITATED OR NEW VEGETATION
- PLANT
- STORMWATER MANAGEMENT POND

**DRAINAGE ASSESSMENT: PHASE 4**

Project Name  
**Freymond Proposed Quarry**

Site  
Bancroft, Ontario

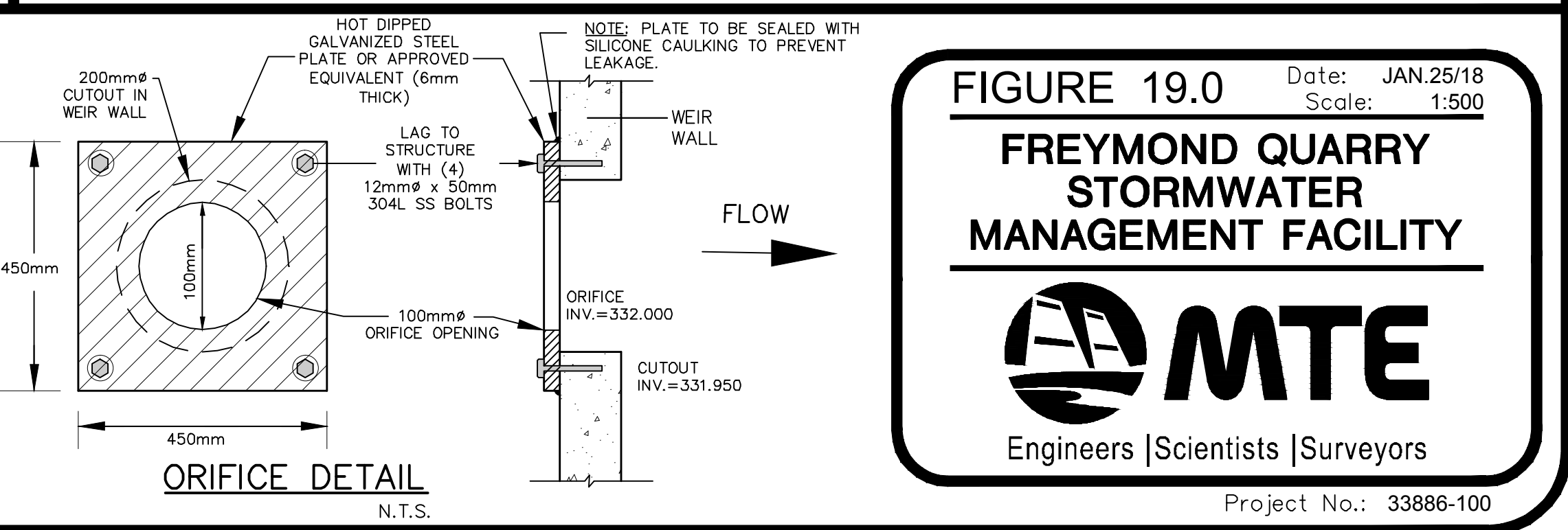
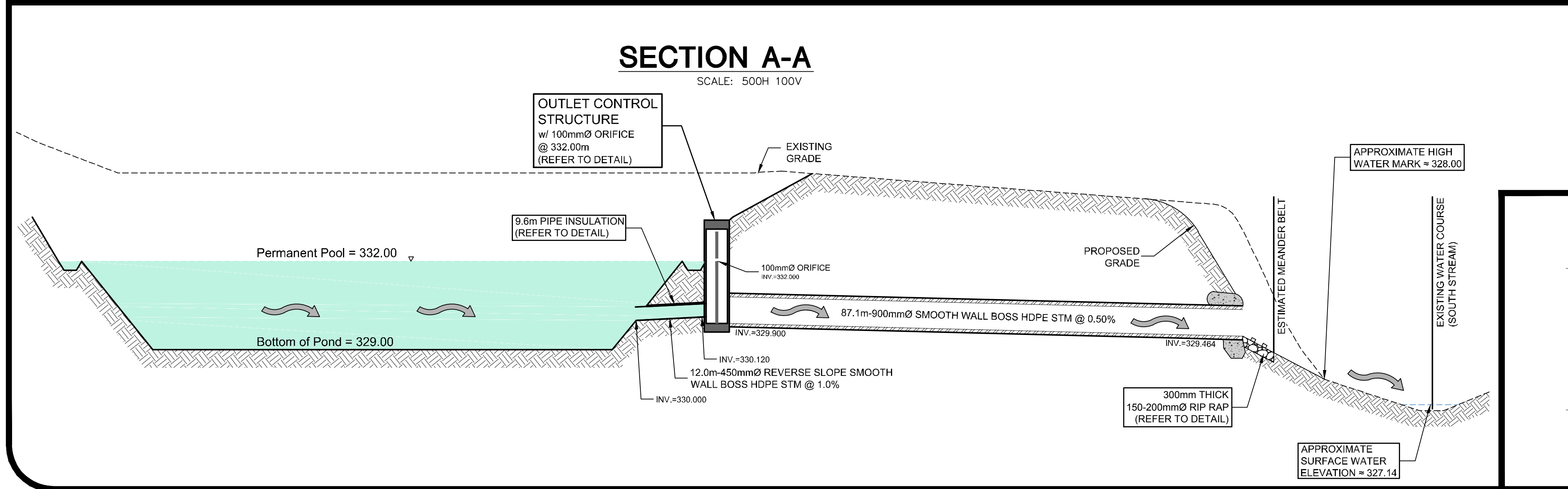
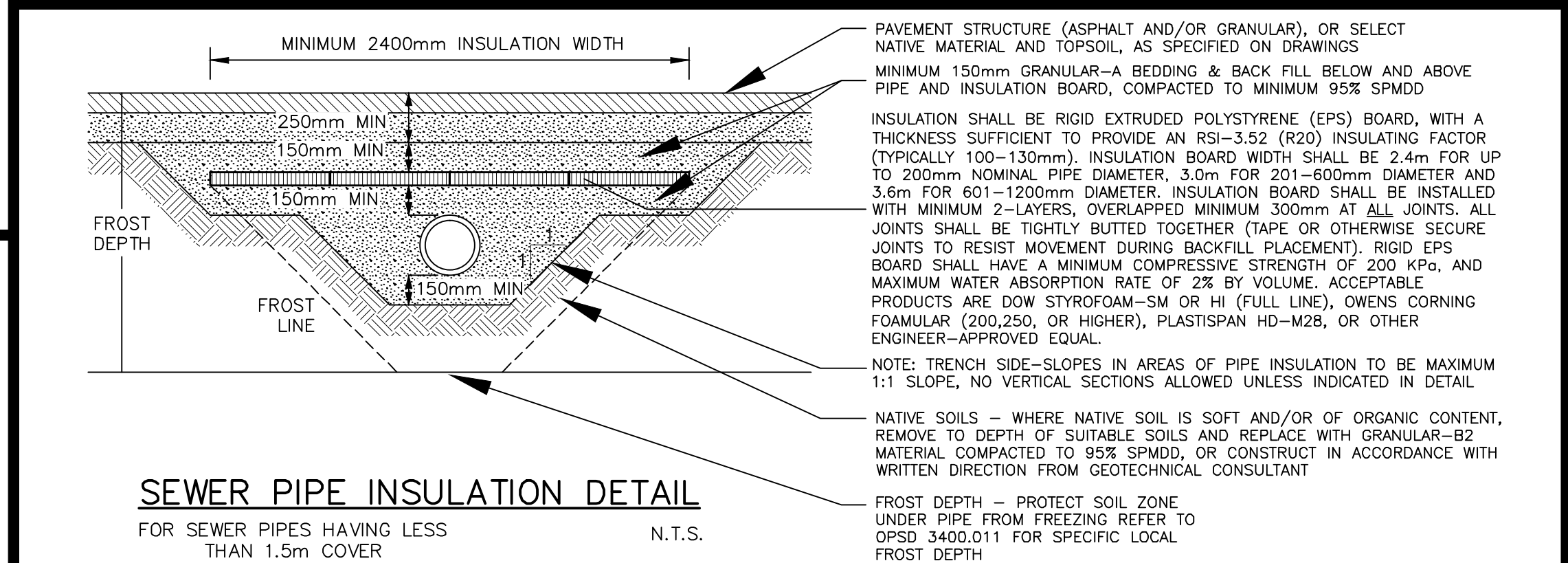
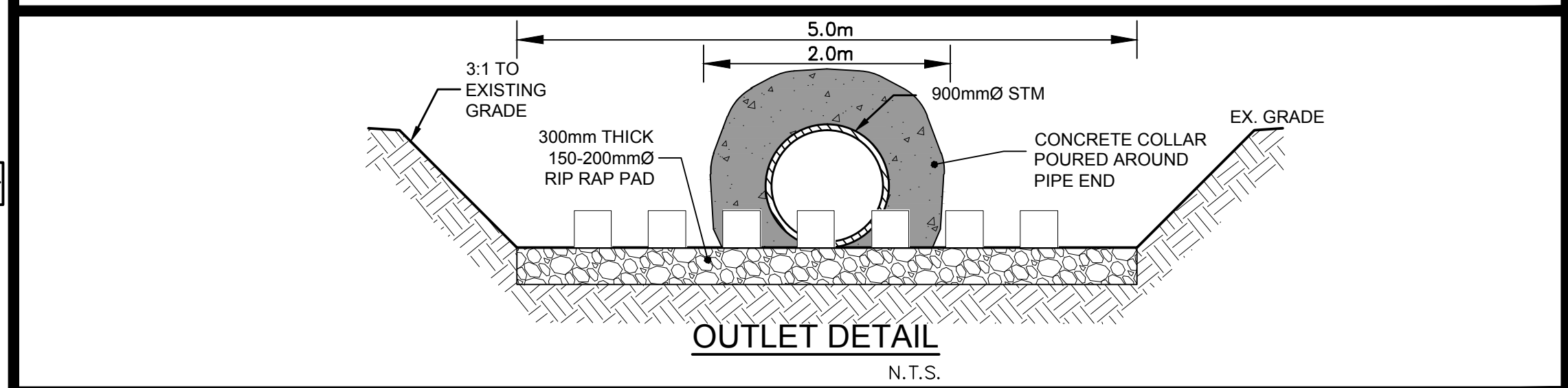
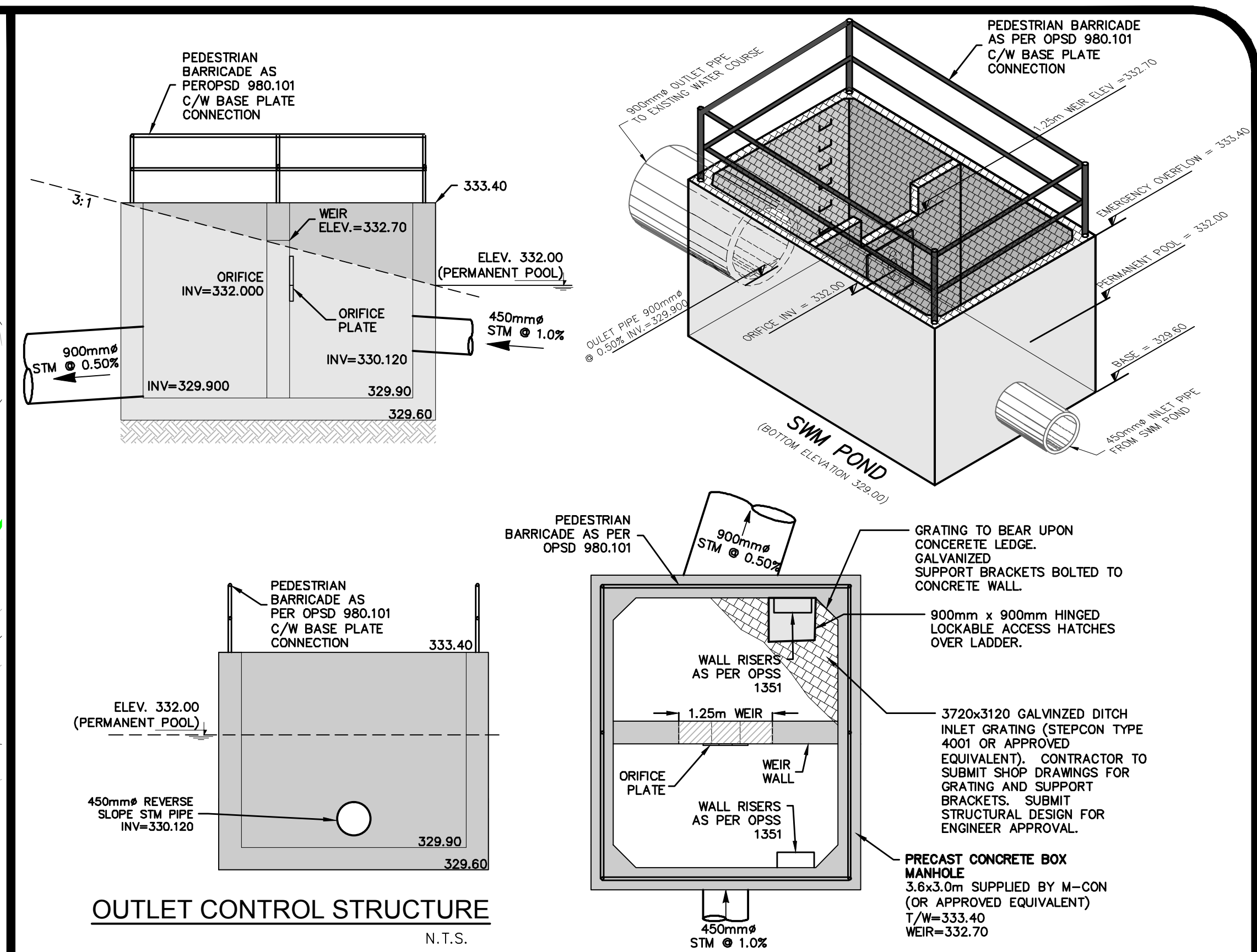
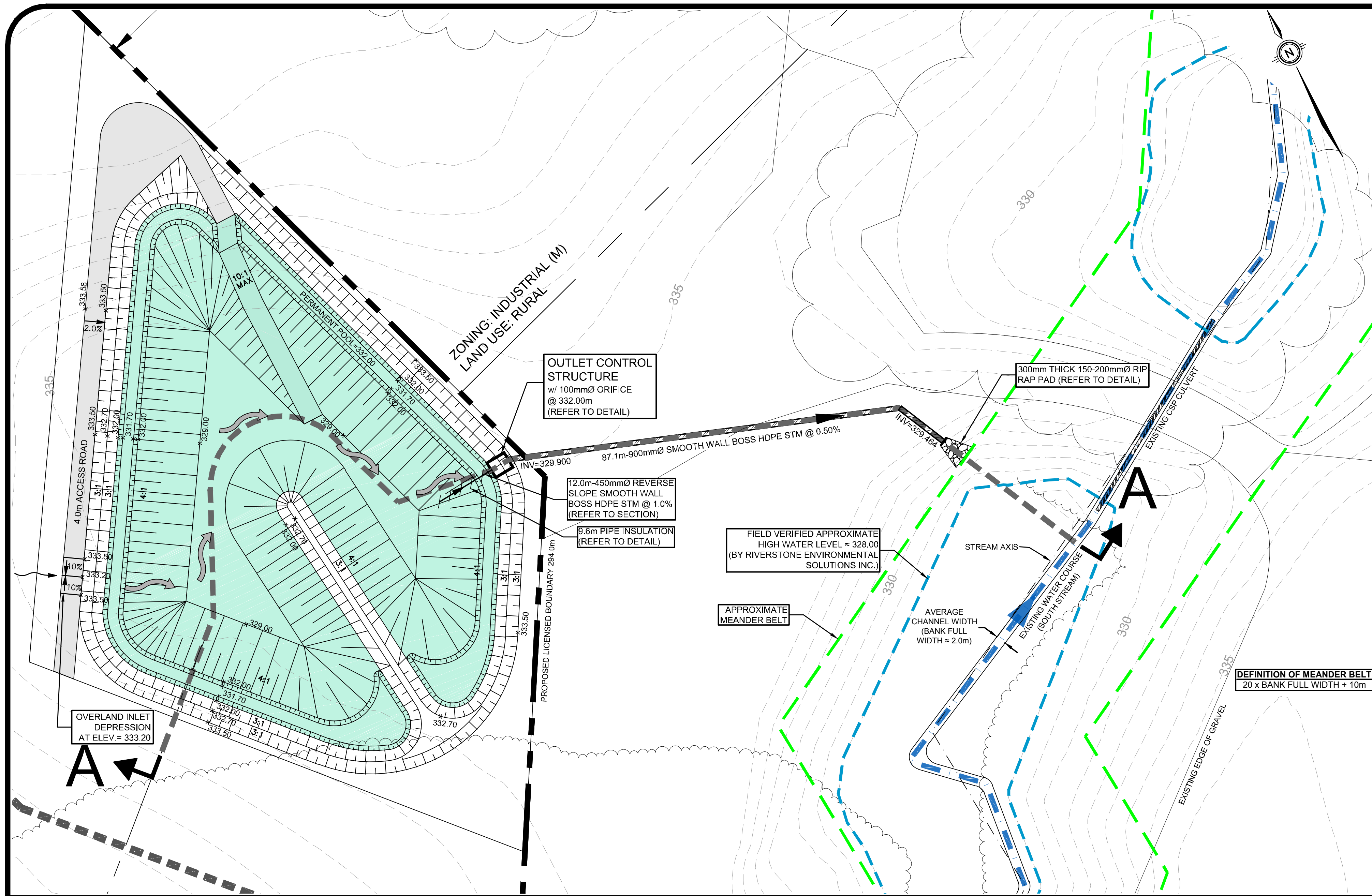
Client  
Freymond Lumber Limited

Scale (11x17)  
1:4000

MTE Project No.  
33886-100

Date  
November 2016

Figure No.  
**18**



**FIGURE 19.0** Date: JAN.25/18 Scale: 1:500

**FREYMOND QUARRY STORMWATER MANAGEMENT FACILITY**

**MTE**  
Engineers | Scientists | Surveyors

Project No.: 33886-100

**FREYMOND QUARRY  
STORMWATER MANAGEMENT  
Bancroft, Ontario**



Project Number: 33886-100  
 Date: June 20, 2017  
 Designer: KMR/CJC  
 File: Q:\33886\Micro Drainage Analysis\SWM\SWM Update - June 2017\33886-100 SWM Design-June 2017.xlsx

**LAND USE CHARACTERISTICS**

	SCS Curve Number			% Imp.
	AMC II	AMC III	Imp.	
Existing Vegetation	81	91	98	0
New Vegetation	81	91	98	15
Rehabilitation/Overburden	81	91	98	100
Excavation/Plant	N/A	N/A	98	100
Stormwater Management	81	91	98	50

**LAND USE BY STAGE**

	Land Use																						
	Existing Vegetation				New Vegetation				Rehabilitation/Overburden				Excavation/Plant				Stormwater Management				TOTAL (area weighted)		
	Area (ha)	Length (m)	Width (m)	Slope (%)	Area (ha)	Length (m)	Width (m)	Slope (%)	Area (ha)	Length (m)	Width (m)	Slope (%)	Area (ha)	Length (m)	Width (m)	Slope (%)	Area (ha)	Length (m)	Width (m)	Slope (%)	Area (ha)	Imp. (%)	Slope (%)
Pre-Excavation	28.88	810	420	7.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	28.88	0.00	7.5
Stage 1	22.47	810	420	7.5	0	0	0	0	5.09	250	200	2	4.75	250	200	1	0.96	120	110	33	33.27	31.02	6.5
Stage 2	14.62	810	220	7.5	4.29	250	200	2	8.23	400	255	2	5.17	240	215	1	0.96	120	110	33	33.27	43.65	5.2
Stage 3 (Design Stage)	5.95	235	220	7.5	9.84	535	200	2	7.53	390	200	2	8.99	390	255	1	0.96	120	110	33	33.27	55.53	3.6
Stage 4	2.8	810	15	7.5	21.46	810	390	2	8.05	185	160	2	0	0	0	0	0.96	120	110	33	33.27	35.31	3.4

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18 " 0.116 Constant B"
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20 " 0.400 Fraction R"
21 " 240.000 Duration"
22 " 1.000 Time step multiplier"
23 " Maximum intensity 88.577 mm/hr"
24 " Total depth 25.008 mm"
25 " 5 25hyd Hydrograph extension used in this file"
26 " 33 CATCHMENT 200"
27 " 1 Triangular SCS"
28 " 1 Equal length"
29 " 1 SCS method"
30 " 200 Site Post-Excavation"
31 " 55.530 % Impervious"
32 " 33.270 Total Area"
33 " 195.000 Flow length"
34 " 3.600 Overland Slope"
35 " 14.795 Pervious Area"
36 " 195.000 Pervious length"
37 " 3.600 Pervious slope"
38 " 18.475 Impervious Area"
39 " 195.000 Impervious length"
40 " 3.600 Impervious slope"
41 " 0.250 Pervious Manning 'n'"
42 " 81.000 Pervious SCS Curve No."
43 " 0.185 Pervious Runoff coefficient"
44 " 0.100 Pervious Ia/S coefficient"
45 " 5.958 Pervious Initial abstraction"
46 " 0.015 Impervious Manning 'n'"
47 " 98.000 Impervious SCS Curve No."
48 " 0.803 Impervious Runoff coefficient"
49 " 0.100 Impervious Ia/S coefficient"
50 " 0.518 Impervious Initial abstraction"
51 " 2.709 0.000 0.000 0.000 c.m/sec"
52 " Catchment 200 Pervious Impervious Total Area "
53 " Surface Area 14.795 18.475 33.270 hectare"
54 " Time of concentration 68.494 6.293 15.964 minutes"
55 " Time to Centroid 243.683 131.293 148.767 minutes"
56 " Rainfall depth 25.008 25.008 25.008 mm"
57 " Rainfall volume 3699.90 4620.10 8320.00 c.m"
58 " Rainfall losses 20.393 4.935 11.809 mm"
59 " Runoff depth 4.615 20.073 13.199 mm"
60 " Runoff volume 682.74 3708.41 4391.15 c.m"
61 " Runoff coefficient 0.185 0.803 0.528 "
62 " Maximum flow 0.061 2.700 2.709 c.m/sec"
63 " 40 HYDROGRAPH Add Runoff "
64 " 4 Add Runoff "
    
```

```

65 " 2.709 2.709 0.000 0.000"
66 " 54 POND DESIGN"
67 " 2.709 Current peak flow c.m/sec"
68 " 0.098 Target outflow c.m/sec"
69 " 4391.1 Hydrograph volume c.m"
70 " 16. Number of stages"
71 " 332.000 Minimum water level metre"
72 " 333.500 Maximum water level metre"
73 " 332.000 Starting water level metre"
74 " 0 Keep Design Data: 1 = True; 0 = False"
75 " Level Discharge Volume"
76 " 332.000 0.000 0.000"
77 " 332.100 0.00400 561.000"
78 " 332.200 0.00800 1134.000"
79 " 332.300 0.01059 1720.000"
80 " 332.400 0.01265 2318.000"
81 " 332.500 0.01443 2928.000"
82 " 332.600 0.01601 3551.000"
83 " 332.700 0.01744 4187.000"
84 " 332.800 0.07940 4840.000"
85 " 332.900 0.1915 5508.000"
86 " 333.000 0.3363 6186.000"
87 " 333.100 0.5075 6874.000"
88 " 333.200 0.7015 7572.000"
89 " 333.300 0.9157 8281.000"
90 " 333.400 1.149 9000.000"
91 " 333.500 1.399 9730.000"
92 " 1. WEIRS"
93 " Crest Weir Crest Left Right"
94 " elevation coefficie breadth sideslope sideslope"
95 " 332.700 0.900 1.250 0.000 0.000"
96 " 1. ORIFICES"
97 " Orifice Orifice Orifice Number of"
98 " invert coefficie diameter orifices"
99 " 332.000 0.630 0.1000 1.000"
100 " Peak outflow 0.017 c.m/sec"
101 " Maximum level 332.680 metre"
102 " Maximum storage 4061.566 c.m"
103 " Centroidal lag 47.961 hours"
104 " 2.709 2.709 0.017 0.000 c.m/sec"
105 " 38 START/RE-START TOTALS 200"
106 " 3 Runoff Totals on EXIT"
107 " Total Catchment area 33.270 hectare"
108 " Total Impervious area 18.475 hectare"
109 " Total % impervious 55.530"
110 " 19 EXIT"
    
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1 " MIDUSS Output ----->"
2 " MIDUSS version Version 2.25 rev. 473"
3 " MIDUSS created Sunday, February 07, 2010"
4 " 10 Units used: ie METRIC"
5 " Job folder: Q:\33886\Micro Drainage Analysis\SWM\
6 " SWM Update - June 2017\MIDUSS"
7 " Output filename: 33886-100-POST-2y.out"
8 " Licensee name: MTE"
9 " Company MTE Consultants Inc."
10 " Date & Time last used: 6/21/2017 at 3:23:33 PM"
11 " 31 TIME PARAMETERS"
12 " 5.000 Time Step"
13 " 240.000 Max. Storm length"
14 " 1500.000 Max. Hydrograph"
15 " 32 STORM Chicago storm"
16 " 1 Chicago storm"
17 " 348.960 Coefficient A"
18 " 0.116 Constant B"
19 " 0.695 Exponent C"
20 " 0.400 Fraction R"
21 " 180.000 Duration"
22 " 1.000 Time step multiplier"
23 " Maximum intensity 112.220 mm/hr"
24 " Total depth 28.333 mm"
25 " 6 002hyd Hydrograph extension used in this file"
26 " 33 CATCHMENT 200"
27 " 1 Triangular SCS"
28 " 1 Equal length"
29 " 1 SCS method"
30 " 200 Site Post-Excavation"
31 " 55.530 % Impervious"
32 " 33.270 Total Area"
33 " 195.000 Flow length"
34 " 3.600 Overland Slope"
35 " 14.795 Pervious Area"
36 " 195.000 Pervious length"
37 " 3.600 Pervious slope"
38 " 18.475 Impervious Area"
39 " 195.000 Impervious length"
40 " 3.600 Impervious slope"
41 " 0.250 Pervious Manning 'n'"
42 " 81.000 Pervious SCS Curve No."
43 " 0.216 Pervious Runoff coefficient"
44 " 0.100 Pervious Ia/S coefficient"
45 " 5.958 Pervious Initial abstraction"
46 " 0.015 Impervious Manning 'n'"
47 " 98.000 Impervious SCS Curve No."
48 " 0.825 Impervious Runoff coefficient"
49 " 0.100 Impervious Ia/S coefficient"
50 " 0.518 Impervious Initial abstraction"
51 " 3.414 0.000 0.000 0.000 c.m/sec"
52 " Catchment 200 Pervious Impervious Total Area "
53 " Surface Area 14.795 18.475 33.270 hectare"
54 " Time of concentration 58.870 5.698 14.904 minutes"
55 " Time to Centroid 187.255 99.633 114.803 minutes"
56 " Rainfall depth 28.333 28.333 28.333 mm"
57 " Rainfall volume 4191.87 5234.42 9426.29 c.m"
58 " Rainfall losses 22.225 4.972 12.644 mm"
59 " Runoff depth 6.108 23.361 15.689 mm"
60 " Runoff volume 903.70 4315.94 5219.64 c.m"
61 " Runoff coefficient 0.216 0.825 0.554 "
62 " Maximum flow 0.105 3.397 3.414 c.m/sec"
63 " 40 HYDROGRAPH Add Runoff "
64 " 4 Add Runoff "
    
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```

65 " 3.414 3.414 0.000 0.000"
66 " 54 POND DESIGN"
67 " 3.414 Current peak flow c.m/sec"
68 " 0.169 Target outflow c.m/sec"
69 " 5219.6 Hydrograph volume c.m"
70 " 16. Number of stages"
71 " 332.000 Minimum water level metre"
72 " 333.500 Maximum water level metre"
73 " 332.000 Starting water level metre"
74 " 0 Keep Design Data: 1 = True; 0 = False"
75 " Level Discharge Volume"
76 " 332.000 0.000 0.000"
77 " 332.100 0.00400 561.000"
78 " 332.200 0.00800 1134.000"
79 " 332.300 0.01059 1720.000"
80 " 332.400 0.01265 2318.000"
81 " 332.500 0.01443 2928.000"
82 " 332.600 0.01601 3551.000"
83 " 332.700 0.01744 4187.000"
84 " 332.800 0.07940 4840.000"
85 " 332.900 0.1915 5508.000"
86 " 333.000 0.3363 6186.000"
87 " 333.100 0.5075 6874.000"
88 " 333.200 0.7015 7572.000"
89 " 333.300 0.9157 8281.000"
90 " 333.400 1.149 9000.000"
91 " 333.500 1.399 9730.000"
92 " 1. WEIRS"
93 " Crest Weir Crest Left Right"
94 " elevation coefficie breadth sideslope sideslope"
95 " 332.700 0.900 1.250 0.000 0.000"
96 " 1. ORIFICES"
97 " Orifice Orifice Orifice Number of"
98 " invert coefficie diameter orifices"
99 " 332.000 0.630 0.1000 1.000"
100 " Peak outflow 0.064 c.m/sec"
101 " Maximum level 332.776 metre"
102 " Maximum storage 4682.029 c.m"
103 " Centroidal lag 43.940 hours"
104 " 3.414 3.414 0.064 0.000 c.m/sec"
105 " 38 START/RE-START TOTALS 200"
106 " 3 Runoff Totals on EXIT"
107 " Total Catchment area 33.270 hectare"
108 " Total Impervious area 18.475 hectare"
109 " Total % impervious 55.530"
110 " 19 EXIT"
    
```

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1 " MIDUSS Output ----->"
2 " MIDUSS version Version 2.25 rev. 473"
3 " MIDUSS created Sunday, February 07, 2010"
4 " 10 Units used: ie METRIC"
5 " Job folder: Q:\33886\Micro Drainage Analysis\SWM\
6 " SWM Update - June 2017\MIDUSS"
7 " Output filename: 33886-100-POST-5y.out"
8 " Licensee name: MTE"
9 " Company MTE Consultants Inc."
10 " Date & Time last used: 6/21/2017 at 3:24:49 PM"
11 " 31 TIME PARAMETERS"
12 " 5.000 Time Step"
13 " 240.000 Max. Storm length"
14 " 1500.000 Max. Hydrograph"
15 " 32 STORM Chicago storm"
16 " 1 Chicago storm"
17 " 464.780 Coefficient A"
18 " 0.019 Constant B"
19 " 0.693 Exponent C"
20 " 0.400 Fraction R"
21 " 180.000 Duration"
22 " 1.000 Time step multiplier"
23 " Maximum intensity 151.957 mm/hr"
24 " Total depth 38.145 mm"
25 " 6 005hyd Hydrograph extension used in this file"
26 " 33 CATCHMENT 200"
27 " 1 Triangular SCS"
28 " 1 Equal length"
29 " 1 SCS method"
30 " 200 Site Post-Excavation"
31 " 55.530 % Impervious"
32 " 33.270 Total Area"
33 " 195.000 Flow length"
34 " 3.600 Overland Slope"
35 " 14.795 Pervious Area"
36 " 195.000 Pervious length"
37 " 3.600 Pervious slope"
38 " 18.475 Impervious Area"
39 " 195.000 Impervious length"
40 " 3.600 Impervious slope"
41 " 0.250 Pervious Manning 'n'"
42 " 81.000 Pervious SCS Curve No."
43 " 0.296 Pervious Runoff coefficient"
44 " 0.100 Pervious Ia/S coefficient"
45 " 5.958 Pervious Initial abstraction"
46 " 0.015 Impervious Manning 'n'"
47 " 98.000 Impervious SCS Curve No."
48 " 0.864 Impervious Runoff coefficient"
49 " 0.100 Impervious Ia/S coefficient"
50 " 0.518 Impervious Initial abstraction"
51 " 4.829 0.000 0.000 0.000 c.m/sec"
52 " Catchment 200 Pervious Impervious Total Area "
53 " Surface Area 14.795 18.475 33.270 hectare"
54 " Time of concentration 43.993 4.970 13.367 minutes"
55 " Time to Centroid 166.745 97.434 112.350 minutes"
56 " Rainfall depth 38.145 38.145 38.145 mm"
57 " Rainfall volume 0.5644 0.7047 1.2691 ha-m"
58 " Rainfall losses 26.861 5.190 14.827 mm"
59 " Runoff depth 11.284 32.955 23.318 mm"
60 " Runoff volume 1669.47 6088.37 7757.83 c.m"
61 " Runoff coefficient 0.296 0.864 0.611 "
62 " Maximum flow 0.259 4.768 4.829 c.m/sec"
63 " 40 HYDROGRAPH Add Runoff "
64 " 4 Add Runoff "
    
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65 " 4.829 4.829 0.000 0.000"
66 " 54 POND DESIGN"
67 " 4.829 Current peak flow c.m/sec"
68 " 0.421 Target outflow c.m/sec"
69 " 7757.8 Hydrograph volume c.m"
70 " 16. Number of stages"
71 " 332.000 Minimum water level metre"
72 " 333.500 Maximum water level metre"
73 " 332.000 Starting water level metre"
74 " 0 Keep Design Data: 1 = True; 0 = False"
75 " Level Discharge Volume"
76 " 332.000 0.000 0.000"
77 " 332.100 0.00400 561.000"
78 " 332.200 0.00800 1134.000"
79 " 332.300 0.01059 1720.000"
80 " 332.400 0.01265 2318.000"
81 " 332.500 0.01443 2928.000"
82 " 332.600 0.01601 3551.000"
83 " 332.700 0.01744 4187.000"
84 " 332.800 0.07940 4840.000"
85 " 332.900 0.1915 5508.000"
86 " 333.000 0.3363 6186.000"
87 " 333.100 0.5075 6874.000"
88 " 333.200 0.7015 7572.000"
89 " 333.300 0.9157 8281.000"
90 " 333.400 1.149 9000.000"
91 " 333.500 1.399 9730.000"
92 " 1. WEIRS"
93 " Crest Weir Crest Left Right"
94 " elevation coefficie breadth sideslope sideslope"
95 " 332.700 0.900 1.250 0.000 0.000"
96 " 1. ORIFICES"
97 " Orifice Orifice Orifice Number of"
98 " invert coefficie diameter orifices"
99 " 332.000 0.630 0.1000 1.000"
100 " Peak outflow 0.288 c.m/sec"
101 " Maximum level 332.967 metre"
102 " Maximum storage 5961.164 c.m"
103 " Centroidal lag 31.778 hours"
104 " 4.829 4.829 0.288 0.000 c.m/sec"
105 " 38 START/RE-START TOTALS 200"
106 " 3 Runoff Totals on EXIT"
107 " Total Catchment area 33.270 hectare"
108 " Total Impervious area 18.475 hectare"
109 " Total % impervious 55.530"
110 " 19 EXIT"
    
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1 " MIDUSS Output ----->"
2 " MIDUSS version Version 2.25 rev. 473"
3 " MIDUSS created Sunday, February 07, 2010"
4 " 10 Units used: ie METRIC"
5 " Job folder: Q:\33886\Micro Drainage Analysis\SWM\
6 " SWM Update - June 2017\MIDUSS"
7 " Output filename: 33886-100-POST-10y.out"
8 " Licensee name: MTE"
9 " Company MTE Consultants Inc."
10 " Date & Time last used: 6/21/2017 at 3:25:18 PM"
11 " 31 TIME PARAMETERS"
12 " 5.000 Time Step"
13 " 240.000 Max. Storm length"
14 " 1500.000 Max. Hydrograph"
15 " 32 STORM Chicago storm"
16 " 1 Chicago storm"
17 " 548.910 Coefficient A"
18 " 0.091 Constant B"
19 " 0.695 Exponent C"
20 " 0.400 Fraction R"
21 " 180.000 Duration"
22 " 1.000 Time step multiplier"
23 " Maximum intensity 177.122 mm/hr"
24 " Total depth 44.571 mm"
25 " 6 010hyd Hydrograph extension used in this file"
26 " 33 CATCHMENT 200"
27 " 1 Triangular SCS"
28 " 1 Equal length"
29 " 1 SCS method"
30 " 200 Site Post-Excavation"
31 " 55.530 % Impervious"
32 " 33.270 Total Area"
33 " 195.000 Flow length"
34 " 3.600 Overland Slope"
35 " 14.795 Pervious Area"
36 " 195.000 Pervious length"
37 " 3.600 Pervious slope"
38 " 18.475 Impervious Area"
39 " 195.000 Impervious length"
40 " 3.600 Impervious slope"
41 " 0.250 Pervious Manning 'n'"
42 " 81.000 Pervious SCS Curve No."
43 " 0.341 Pervious Runoff coefficient"
44 " 0.100 Pervious Ia/S coefficient"
45 " 5.958 Pervious Initial abstraction"
46 " 0.015 Impervious Manning 'n'"
47 " 98.000 Impervious SCS Curve No."
48 " 0.880 Impervious Runoff coefficient"
49 " 0.100 Impervious Ia/S coefficient"
50 " 0.518 Impervious Initial abstraction"
51 " 5.738 0.000 0.000 0.000 c.m/sec"
52 " Catchment 200 Pervious Impervious Total Area "
53 " Surface Area 14.795 18.475 33.270 hectare"
54 " Time of concentration 38.540 4.646 12.664 minutes"
55 " Time to Centroid 158.383 96.345 111.020 minutes"
56 " Rainfall depth 44.571 44.571 44.571 mm"
57 " Rainfall volume 0.6594 0.8234 1.4829 ha-m"
58 " Rainfall losses 29.393 5.340 16.036 mm"
59 " Runoff depth 15.178 39.232 28.535 mm"
60 " Runoff volume 2245.68 7248.01 9493.68 c.m"
61 " Runoff coefficient 0.341 0.880 0.640 "
62 " Maximum flow 0.404 5.630 5.738 c.m/sec"
63 " 40 HYDROGRAPH Add Runoff "
64 " 4 Add Runoff "
    
```

```

65 " 5.738 5.738 0.000 0.000"
66 " 54 POND DESIGN"
67 " 5.738 Current peak flow c.m/sec"
68 " 0.653 Target outflow c.m/sec"
69 " 9493.7 Hydrograph volume c.m"
70 " 16. Number of stages"
71 " 332.000 Minimum water level metre"
72 " 333.500 Maximum water level metre"
73 " 332.000 Starting water level metre"
74 " 0 Keep Design Data: 1 = True; 0 = False"
75 " Level Discharge Volume"
76 " 332.000 0.000 0.000"
77 " 332.100 0.00400 561.000"
78 " 332.200 0.00800 1134.000"
79 " 332.300 0.01059 1720.000"
80 " 332.400 0.01265 2318.000"
81 " 332.500 0.01443 2928.000"
82 " 332.600 0.01601 3551.000"
83 " 332.700 0.01744 4187.000"
84 " 332.800 0.07940 4840.000"
85 " 332.900 0.1915 5508.000"
86 " 333.000 0.3363 6186.000"
87 " 333.100 0.5075 6874.000"
88 " 333.200 0.7015 7572.000"
89 " 333.300 0.9157 8281.000"
90 " 333.400 1.149 9000.000"
91 " 333.500 1.399 9730.000"
92 " 1. WEIRS"
93 " Crest Weir Crest Left Right"
94 " elevation coefficie breadth sideslope sideslope"
95 " 332.700 0.900 1.250 0.000 0.000"
96 " 1. ORIFICES"
97 " Orifice Orifice Orifice Number of"
98 " invert coefficie diameter orifices"
99 " 332.000 0.630 0.1000 1.000"
100 " Peak outflow 0.443 c.m/sec"
101 " Maximum level 333.063 metre"
102 " Maximum storage 6616.882 c.m"
103 " Centroidal lag 26.703 hours"
104 " 5.738 5.738 0.443 0.000 c.m/sec"
105 " 38 START/RE-START TOTALS 200"
106 " 3 Runoff Totals on EXIT"
107 " Total Catchment area 33.270 hectare"
108 " Total Impervious area 18.475 hectare"
109 " Total % impervious 55.530"
110 " 19 EXIT"
    
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1 " MIDUSS Output ----->"
2 " MIDUSS version Version 2.25 rev. 473"
3 " MIDUSS created Sunday, February 07, 2010"
4 " 10 Units used: ie METRIC"
5 " Job folder: Q:\33886\Micro Drainage Analysis\SWM\
6 " SWM Update - June 2017\MIDUSS"
7 " Output filename: 33886-100-POST-25y.out"
8 " Licensee name: MTE"
9 " Company MTE Consultants Inc."
10 " Date & Time last used: 6/21/2017 at 3:25:43 PM"
11 " 31 TIME PARAMETERS"
12 " 5.000 Time Step"
13 " 240.000 Max. Storm length"
14 " 1500.000 Max. Hydrograph"
15 " 32 STORM Chicago storm"
16 " 1 Chicago storm"
17 " 641.060 Coefficient A"
18 " 0.011 Constant B"
19 " 0.692 Exponent C"
20 " 0.400 Fraction R"
21 " 180.000 Duration"
22 " 1.000 Time step multiplier"
23 " Maximum intensity 210.160 mm/hr"
24 " Total depth 52.888 mm"
25 " 6 025hyd Hydrograph extension used in this file"
26 " 33 CATCHMENT 200"
27 " 1 Triangular SCS"
28 " 1 Equal length"
29 " 1 SCS method"
30 " 200 Site Post-Excavation"
31 " 55.530 % Impervious"
32 " 33.270 Total Area"
33 " 195.000 Flow length"
34 " 3.600 Overland Slope"
35 " 14.795 Pervious Area"
36 " 195.000 Pervious length"
37 " 3.600 Pervious slope"
38 " 18.475 Impervious Area"
39 " 195.000 Impervious length"
40 " 3.600 Impervious slope"
41 " 0.250 Pervious Manning 'n'"
42 " 81.000 Pervious SCS Curve No."
43 " 0.391 Pervious Runoff coefficient"
44 " 0.100 Pervious Ia/S coefficient"
45 " 5.958 Pervious Initial abstraction"
46 " 0.015 Impervious Manning 'n'"
47 " 98.000 Impervious SCS Curve No."
48 " 0.893 Impervious Runoff coefficient"
49 " 0.100 Impervious Ia/S coefficient"
50 " 0.518 Impervious Initial abstraction"
51 " 6.759 0.000 0.000 0.000 c.m/sec"
52 " Catchment 200 Pervious Impervious Total Area "
53 " Surface Area 14.795 18.475 33.270 hectare"
54 " Time of concentration 33.630 4.317 11.924 minutes"
55 " Time to Centroid 150.862 95.418 109.807 minutes"
56 " Rainfall depth 52.888 52.888 52.888 mm"
57 " Rainfall volume 0.7825 0.9771 1.7596 ha-m"
58 " Rainfall losses 32.212 5.646 17.460 mm"
59 " Runoff depth 20.675 47.242 35.428 mm"
60 " Runoff volume 0.3059 0.8728 1.1787 ha-m"
61 " Runoff coefficient 0.391 0.893 0.670 "
62 " Maximum flow 0.616 6.563 6.759 c.m/sec"
63 " 40 HYDROGRAPH Add Runoff "
64 " 4 Add Runoff "
    
```

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65 " 6.759 6.759 0.000 0.000"
66 " 54 POND DESIGN"
67 " 6.759 Current peak flow c.m/sec"
68 " 0.982 Target outflow c.m/sec"
69 " 11786.8 Hydrograph volume c.m"
70 " 16. Number of stages"
71 " 332.000 Minimum water level metre"
72 " 333.500 Maximum water level metre"
73 " 332.000 Starting water level metre"
74 " 0 Keep Design Data: 1 = True; 0 = False"
75 " Level Discharge Volume"
76 " 332.000 0.000 0.000"
77 " 332.100 0.00400 561.000"
78 " 332.200 0.00800 1134.000"
79 " 332.300 0.01059 1720.000"
80 " 332.400 0.01265 2318.000"
81 " 332.500 0.01443 2928.000"
82 " 332.600 0.01601 3551.000"
83 " 332.700 0.01744 4187.000"
84 " 332.800 0.07940 4840.000"
85 " 332.900 0.1915 5508.000"
86 " 333.000 0.3363 6186.000"
87 " 333.100 0.5075 6874.000"
88 " 333.200 0.7015 7572.000"
89 " 333.300 0.9157 8281.000"
90 " 333.400 1.149 9000.000"
91 " 333.500 1.399 9730.000"
92 " 1. WEIRS"
93 " Crest Weir Crest Left Right"
94 " elevation coefficie breadth sideslope sideslope"
95 " 332.700 0.900 1.250 0.000 0.000"
96 " 1. ORIFICES"
97 " Orifice Orifice Orifice Number of"
98 " invert coefficie diameter orifices"
99 " 332.000 0.630 0.1000 1.000"
100 " Peak outflow 0.680 c.m/sec"
101 " Maximum level 333.189 metre"
102 " Maximum storage 7494.173 c.m"
103 " Centroidal lag 22.179 hours"
104 " 6.759 6.759 0.680 0.000 c.m/sec"
105 " 38 START/RE-START TOTALS 200"
106 " 3 Runoff Totals on EXIT"
107 " Total Catchment area 33.270 hectare"
108 " Total Impervious area 18.475 hectare"
109 " Total % impervious 55.530"
110 " 19 EXIT"
    
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1 " MIDUSS Output ----->"
2 " MIDUSS version Version 2.25 rev. 473"
3 " MIDUSS created Sunday, February 07, 2010"
4 " 10 Units used: ie METRIC"
5 " Job folder: Q:\33886\Micro Drainage Analysis\SWM\
6 " SWM Update - June 2017\MIDUSS"
7 " Output filename: 33886-100-POST-50y.out"
8 " Licensee name: MTE"
9 " Company MTE Consultants Inc."
10 " Date & Time last used: 6/21/2017 at 3:26:09 PM"
11 " 31 TIME PARAMETERS"
12 " 5.000 Time Step"
13 " 240.000 Max. Storm length"
14 " 1500.000 Max. Hydrograph"
15 " 32 STORM Chicago storm"
16 " 1 Chicago storm"
17 " 721.060 Coefficient A"
18 " 0.031 Constant B"
19 " 0.695 Exponent C"
20 " 0.400 Fraction R"
21 " 180.000 Duration"
22 " 1.000 Time step multiplier"
23 " Maximum intensity 234.597 mm/hr"
24 " Total depth 58.563 mm"
25 " 6 050hyd Hydrograph extension used in this file"
26 " 33 CATCHMENT 200"
27 " 1 Triangular SCS"
28 " 1 Equal length"
29 " 1 SCS method"
30 " 200 Site Post-Excavation"
31 " 55.530 % Impervious"
32 " 33.270 Total Area"
33 " 195.000 Flow length"
34 " 3.600 Overland Slope"
35 " 14.795 Pervious Area"
36 " 195.000 Pervious length"
37 " 3.600 Pervious slope"
38 " 18.475 Impervious Area"
39 " 195.000 Impervious length"
40 " 3.600 Impervious slope"
41 " 0.250 Pervious Manning 'n'"
42 " 81.000 Pervious SCS Curve No."
43 " 0.421 Pervious Runoff coefficient"
44 " 0.100 Pervious Ia/S coefficient"
45 " 5.958 Pervious Initial abstraction"
46 " 0.015 Impervious Manning 'n'"
47 " 98.000 Impervious SCS Curve No."
48 " 0.898 Impervious Runoff coefficient"
49 " 0.100 Impervious Ia/S coefficient"
50 " 0.518 Impervious Initial abstraction"
51 " 7.603 0.000 0.000 0.000 c.m/sec"
52 " Catchment 200 Pervious Impervious Total Area "
53 " Surface Area 14.795 18.475 33.270 hectare"
54 " Time of concentration 31.038 4.121 11.465 minutes"
55 " Time to Centroid 146.549 94.772 108.901 minutes"
56 " Rainfall depth 58.563 58.563 58.563 mm"
57 " Rainfall volume 0.8665 1.0819 1.9484 ha-m"
58 " Rainfall losses 33.906 5.945 18.379 mm"
59 " Runoff depth 24.657 52.619 40.184 mm"
60 " Runoff volume 0.3648 0.9721 1.3369 ha-m"
61 " Runoff coefficient 0.421 0.898 0.686 "
62 " Maximum flow 0.819 7.327 7.603 c.m/sec"
63 " 40 HYDROGRAPH Add Runoff "
64 " 4 Add Runoff "
    
```

```

65 " 7.603 7.603 0.000 0.000"
66 " 54 POND DESIGN"
67 " 7.603 Current peak flow c.m/sec"
68 " 1.314 Target outflow c.m/sec"
69 " 13369.2 Hydrograph volume c.m"
70 " 16. Number of stages"
71 " 332.000 Minimum water level metre"
72 " 333.500 Maximum water level metre"
73 " 332.000 Starting water level metre"
74 " 0 Keep Design Data: 1 = True; 0 = False"
75 " Level Discharge Volume"
76 " 332.000 0.000 0.000"
77 " 332.100 0.00400 561.000"
78 " 332.200 0.00800 1134.000"
79 " 332.300 0.01059 1720.000"
80 " 332.400 0.01265 2318.000"
81 " 332.500 0.01443 2928.000"
82 " 332.600 0.01601 3551.000"
83 " 332.700 0.01744 4187.000"
84 " 332.800 0.07940 4840.000"
85 " 332.900 0.1915 5508.000"
86 " 333.000 0.3363 6186.000"
87 " 333.100 0.5075 6874.000"
88 " 333.200 0.7015 7572.000"
89 " 333.300 0.9157 8281.000"
90 " 333.400 1.149 9000.000"
91 " 333.500 1.399 9730.000"
92 " 1. WEIRS"
93 " Crest Weir Crest Left Right"
94 " elevation coefficient breadth sideslope sideslope"
95 " 332.700 0.900 1.250 0.000 0.000"
96 " 1. ORIFICES"
97 " Orifice Orifice Orifice Number of"
98 " invert coefficient diameter orifices"
99 " 332.000 0.630 0.1000 1.000"
100 " Peak outflow 0.873 c.m/sec"
101 " Maximum level 333.280 metre"
102 " Maximum storage 8138.307 c.m"
103 " Centroidal lag 19.953 hours"
104 " 7.603 7.603 0.873 0.000 c.m/sec"
105 " 38 START/RE-START TOTALS 200"
106 " 3 Runoff Totals on EXIT"
107 " Total Catchment area 33.270 hectare"
108 " Total Impervious area 18.475 hectare"
109 " Total % impervious 55.530"
110 " 19 EXIT"
    
```

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1 " MIDUSS Output ----->"
2 " MIDUSS version Version 2.25 rev. 473"
3 " MIDUSS created Sunday, February 07, 2010"
4 " 10 Units used: ie METRIC"
5 " Job folder: Q:\33886\Micro Drainage Analysis\SWM\
6 " SWM Update - June 2017\MIDUSS"
7 " Output filename: 33886-100-POST-100y.out"
8 " Licensee name: MTE"
9 " Company MTE Consultants Inc."
10 " Date & Time last used: 6/21/2017 at 3:27:03 PM"
11 " 31 TIME PARAMETERS"
12 " 5.000 Time Step"
13 " 240.000 Max. Storm length"
14 " 1500.000 Max. Hydrograph"
15 " 32 STORM Chicago storm"
16 " 1 Chicago storm"
17 " 797.520 Coefficient A"
18 " 0.036 Constant B"
19 " 0.695 Exponent C"
20 " 0.400 Fraction R"
21 " 180.000 Duration"
22 " 1.000 Time step multiplier"
23 " Maximum intensity 259.294 mm/hr"
24 " Total depth 64.772 mm"
25 " 6 100hyd Hydrograph extension used in this file"
26 " 33 CATCHMENT 200"
27 " 1 Triangular SCS"
28 " 1 Equal length"
29 " 1 SCS method"
30 " 200 Site Post-Excavation"
31 " 55.530 % Impervious"
32 " 33.270 Total Area"
33 " 195.000 Flow length"
34 " 3.600 Overland Slope"
35 " 14.795 Pervious Area"
36 " 195.000 Pervious length"
37 " 3.600 Pervious slope"
38 " 18.475 Impervious Area"
39 " 195.000 Impervious length"
40 " 3.600 Impervious slope"
41 " 0.250 Pervious Manning 'n'"
42 " 81.000 Pervious SCS Curve No."
43 " 0.451 Pervious Runoff coefficient"
44 " 0.100 Pervious Ia/S coefficient"
45 " 5.958 Pervious Initial abstraction"
46 " 0.015 Impervious Manning 'n'"
47 " 98.000 Impervious SCS Curve No."
48 " 0.902 Impervious Runoff coefficient"
49 " 0.100 Impervious Ia/S coefficient"
50 " 0.518 Impervious Initial abstraction"
51 " 8.477 0.000 0.000 0.000 c.m/sec"
52 " Catchment 200 Pervious Impervious Total Area "
53 " Surface Area 14.795 18.475 33.270 hectare"
54 " Time of concentration 28.855 3.950 11.067 minutes"
55 " Time to Centroid 142.929 94.228 108.146 minutes"
56 " Rainfall depth 64.772 64.772 64.772 mm"
57 " Rainfall volume 0.9583 1.1967 2.1550 ha-m"
58 " Rainfall losses 35.587 6.359 19.357 mm"
59 " Runoff depth 29.185 58.413 45.415 mm"
60 " Runoff volume 0.4318 1.0792 1.5110 ha-m"
61 " Runoff coefficient 0.451 0.902 0.701 "
62 " Maximum flow 1.020 8.097 8.477 c.m/sec"
63 " 40 HYDROGRAPH Add Runoff "
64 " 4 Add Runoff "
    
```

```

65 " 8.477 8.477 0.000 0.000"
66 " 54 POND DESIGN"
67 " 8.477 Current peak flow c.m/sec"
68 " 1.639 Target outflow c.m/sec"
69 " 15109.7 Hydrograph volume c.m"
70 " 16. Number of stages"
71 " 332.000 Minimum water level metre"
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73 " 332.000 Starting water level metre"
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75 " Level Discharge Volume"
76 " 332.000 0.000 0.000"
77 " 332.100 0.00400 561.000"
78 " 332.200 0.00800 1134.000"
79 " 332.300 0.01059 1720.000"
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81 " 332.500 0.01443 2928.000"
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83 " 332.700 0.01744 4187.000"
84 " 332.800 0.07940 4840.000"
85 " 332.900 0.1915 5508.000"
86 " 333.000 0.3363 6186.000"
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96 " 1. ORIFICES"
97 " Orifice Orifice Orifice Number of"
98 " invert coefficie diameter orifices"
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103 " Centroidal lag 17.997 hours"
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109 " Total % impervious 55.530"
110 " 19 EXIT"
    
```

**FREYMOND QUARRY**  
**STORMWATER MANAGEMENT**  
 Bancroft, Ontario



Project Number: 33886-100  
 Date: June 20, 2017  
 Designer: KMR/CJC  
 File: Q:\33886\Micro Drainage Analysis\SWM\SWM Update - June 2017\33886-100 SWM Design-June 2017.xlsx

**QUANTITY CONTROL MODELING SUMMARY (Permanent Pool = 332.00m)**

Storm Event	Pre-Excavation Peak Flow (m <sup>3</sup> /s)	Pre-Excavation Runoff Volume (m <sup>3</sup> )	Post-Excavation Pond Inflow (m <sup>3</sup> /s)	Post-Excavation Runoff Volume (m <sup>3</sup> )	Post-Excavation Pond Outflow (m <sup>3</sup> /s)	Required Storage Volume (m <sup>3</sup> )	Peak Ponding Elevation (m)
25mm	0.098	1333	2.709	4392	0.017	4062	332.68
2 Year	0.169	1765	3.414	5220	0.064	4682	332.78
5 Year	0.421	3260	4.829	7758	0.288	5961	332.97
10 Year	0.653	4385	5.738	9494	0.443	6617	333.06
25 Year	0.982	5972	6.759	11787	0.680	7494	333.19
50 Year	1.314	7124	7.603	13370	0.873	8138	333.28
100 Year	1.639	8438	8.477	15110	1.098	8845	333.38

**IDF PARAMETERS - MTO Curve Lookup Application; Bancroft**

Frequency	a	b	c	t <sub>TOTAL</sub> (min.)
25mm	282.1	0.116	0.6954	240
2 Year	348.96	0.116	0.6954	180
5 Year	464.78	0.019	0.6928	180
10 Year	548.91	0.091	0.6948	180
25 Year	641.06	0.011	0.6923	180
50 Year	721.06	0.031	0.6946	180
100 Year	797.52	0.036	0.6954	180

$Intensity = a / (t + b)^c$

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**FALLING HEAD DRAWDOWN CALCULATION**  
 MOEE SWM Planning and Design Manual, 2003

$$t = \frac{0.66C_2h^{1.5} + 2C_3h^{0.5}}{2.75A_o} \quad \text{Equation 4.11}$$

where

t =	255431 s	
	71.0 hr	drawdown time
A <sub>p</sub> =	5947.02 m <sup>2</sup>	surface area of the pond
C =	0.63	discharge coefficient
d =	100 mm	diameter of the orifice
A <sub>o</sub> =	0.00785 m <sup>2</sup>	cross-sectional area of the orifice
g =	9.81 m/s <sup>2</sup>	gravitational acceleration constant
h <sub>1</sub> =	332.230 m	starting water elevation above the orifice
h <sub>2</sub> =	332.000 m	ending water elevation above the orifice
h =	0.23 m	maximum water elevation above the orifice
C <sub>2</sub> =	1266.94	slope coefficient from the area-depth linear regression
C <sub>3</sub> =	5655.62	intercept from the area-depth linear regression

	ELEVATION m	STAGE m	AREA m <sup>2</sup>	COMMENTS
1	332.000	0	5656.8	
2	332.100	0.1	5782.1	
3	332.200	0.2	5908.1	
4	332.300	0.3	6034.7	
5	332.400	0.4	6162.2	
6	332.500	0.5	6290.3	

**DRAWDOWN TIME:** 255431 s  
71.0 hr

**Regression Output:**

m <sub>1</sub> =	1266.94	slope coefficient from the area-depth linear regression
b =	5655.62	intercept from the area-depth linear regression
se <sub>m1</sub> =	2.59	standard error for coefficient m <sub>1</sub>
se <sub>b</sub> =	0.79	standard error for constant b
R <sup>2</sup> =	1.0000	coefficient of determination
se <sub>y</sub> =	1.08	standard error of the y estimate
F =	2.39E+05	F statistic
df =	4	degrees of freedom
SS <sub>reg</sub> =	280899	regression sum of squares
SS <sub>resid</sub> =	5	residual sum of squares



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**SETTLING CALCULATIONS**

MOE SWM Planning and Design Manual, 2003

**Design Flows**

Peak flow into facility during the 1:100-year return period event **8.477 m<sup>3</sup>/s**  
 Peak flow into facility during the 25 mm - 4 hour design storm event **2.709 m<sup>3</sup>/s**  
 Peak flow from facility outlet for the 25 mm - 4 hour design storm event **0.017 m<sup>3</sup>/s**

**Facility Characteristics**

b = **5.0 m** bottom width  
 y = **3 m** 25mm storm storage depth  
 z = **4 :1** side slope  
 w = **17.0 m** average width  
 R = **1.71 m** hydraulic radius  
 A = **51.0 m<sup>2</sup>** cross-sectional area

**1. Length Calculation Based on Settling Velocity**

L = facility flow length (m)  
 r = length-to-width ratio  
 Q<sub>p</sub> = peak flow rate through facility (m<sup>3</sup>/s)  
 v<sub>s</sub> = settling velocity (m/s)

$$L = \sqrt{\frac{rQ_p}{v_s}} \quad \text{Equation 4.5: Forebay Settling Length}$$

**a) Required Settling Length (assuming Q<sub>p</sub> = pond discharge & v<sub>s</sub> = 0.00002540 m/s)**

Q<sub>p</sub> = 0.017 m<sup>3</sup>/s peak flow rate through facility  
 v<sub>s</sub> = 0.00002540 m/s settling velocity  
 r = 2.31 length-to-width ratio  
 L = **39.3 m** required settling length  
 L = **39.3 m** trial length

**Table 1: Average settling velocities**

Mass Removed	Particle Size Range	Average Settling Velocity	
%	µm	m/s	
Enhanced:	80 - 100	x ≤ 20	0.00000254
	70 - 80	20 < x ≤ 40	0.00001300
Normal:	60 - 70	40 < x ≤ 60	0.00002540
Basic:	40 - 60	60 < x ≤ 130	0.00012700
Medium Sand:	20 - 40	130 < x ≤ 400	0.00059267
Gross Grit:	0 - 20	400 < x ≤ 4000	0.00550333

**b) Required Settling Length (assuming Q<sub>p</sub> = pond discharge & v<sub>s</sub> = 0.00001300 m/s)**

Q<sub>p</sub> = 0.017 m<sup>3</sup>/s peak flow rate through facility  
 v<sub>s</sub> = 0.00001300 m/s settling velocity  
 r = 4.52 length-to-width ratio  
 L = **76.9 m** required settling length  
 L = **76.9 m** trial length

**2. Length Calculation Based on Flow Dispersion Length**

Q = 8.48 m<sup>3</sup>/s peak inlet flow rate  
 d = 3 m depth of permanent pool in facility  
 V<sub>f</sub> = 0.50 m/s desired velocity in facility (typical value ≤ 0.50 m/s)  
 L = **45.2 m** required length of dispersion

$$L_D = \frac{8Q}{dV_f} \quad \text{Equation 4.6: Dispersion Length}$$

**3. Required Facility Length**

L = **76.9 m** **design length**  
 r = 4.52 design length-to-width ratio (typical minimum of 2.0)

**4. Scour Velocity**

v<sub>s</sub> = **0.15 m/s** scour velocity (typical value = 0.15 m/s)  
 v = **0.166 m/s** **actual velocity** **ERROR! ERROR!** The actual velocity through the facility exceeds the scour velocity

**5. Estimated Cleanout Frequency**

**Facility**

Spare permanent pool volume beyond requirement **2648 m<sup>3</sup>**  
 Estimated TSS removal efficiency **80%**  
 Impervious level **56%**  
 Estimated annual sediment loading **1.9 m<sup>3</sup>/ha**  
 Contributing area **33.27 ha**  
 Annual sediment volume **51 m<sup>3</sup>/yr**  
**Frequency for 100% spare volume reduction 52.4 years**

**Table 2: Annual sediment loading**

Impervious Level	Annual Loading
%	m <sup>3</sup> /ha
35%	0.6
55%	1.9
70%	2.8
85%	3.8

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**Step 1: Choose Level of Water Quality Control**

Enhanced 80% long-term S.S. removal

**Step 2: Choose Type of Facility**

Wet Pond

**Step 3: Define Catchment area and Imperviousness**

Catchment Area (ha)

Imperviousness (%)

33.27

55.53

Interpolated Storage Volume Requirement (m<sup>3</sup>/ha)

191.24

Permanent Pool Required (m<sup>3</sup>)

5031.92

Extended Detention Volume Required (m<sup>3</sup>)

1330.80

Protection Level	SWMP Type	Storage Volume (m <sup>3</sup> /ha) for Impervious Level			
		35	55	70	85
Enhanced 80% long-term S.S. removal	Wetlands	80	105	120	140
	Hybrid Wet Pond/Wetland	110	150	175	195
	Wet Pond	140	190	225	250
Normal 70% long-term S.S. Removal	Wetlands	60	70	80	90
	Hybrid Wet Pond/Wetland	75	90	105	120
	Wet Pond	90	110	130	150
Basic 60% long-term S.S. Removal	Wetlands	60	60	60	60
	Hybrid Wet Pond/Wetland	60	70	75	80
	Wet Pond	60	75	85	95
	Dry Pond (Continuous Flow)	90	150	200	240

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**STAGE-STORAGE RELATIONSHIP - WET POND**

Stage	Active Depth	Main Pond			Total Pond Volume	Active Storage Volume	Total Outflow*	Volume Summary	Ponding Elevation	Comments	Stage
		Area	Volume	Cumulative Volume							
m	m	m <sup>2</sup>	m <sup>3</sup>	m <sup>3</sup>	m <sup>3</sup>	m <sup>3</sup>	m <sup>3</sup> /s	m <sup>3</sup>	m		m
329.00		758	0	0	0		*from				329.00
329.10		859	81	81	81		MIDUSS				329.10
329.20		963	91	172	172						329.20
329.30		1070	102	274	274						329.30
329.40		1178	112	386	386						329.40
329.50		1290	123	509	509		100mm				329.50
329.60		1404	135	644	644		orifice				329.60
329.70		1520	146	790	790		@ 332.00m				329.70
329.80		1639	158	948	948		+				329.80
329.90		1760	170	1118	1118		1.25m				329.90
330.00		1883	182	1300	1300		weir				330.00
330.10		2006	194	1495	1495		@ 332.70m				330.10
330.20		2132	207	1702	1702						330.20
330.30		2258	219	1921	1921						330.30
330.40		2386	232	2153	2153						330.40
330.50		2515	245	2398	2398						330.50
330.60		2645	258	2656	2656						330.60
330.70		2777	271	2928	2928						330.70
330.80		2908	284	3212	3212						330.80
330.90		3040	297	3509	3509						330.90
331.00		3174	311	3820	3820						331.00
331.10		3308	324	4144	4144						331.10
331.20		3443	338	4482	4482						331.20
331.30		3580	351	4833	4833						331.30
331.40		3717	365	5198	5198						331.40
331.50		3856	379	5576	5576						331.50
331.60		3995	393	5969	5969						331.60
331.70		4135	407	6375	6375						331.70
331.80		4277	421	6796	6796						331.80
331.90		4419	435	7231	7231						331.90
332.00		4563	449	7680	7680			7680		Permanent Pool	332.00
332.00	0.00	5549	296	7975	7975	0	0.000				332.00
332.10	0.10	5671	561	8536	8536	561	0.004				332.10
332.20	0.20	5794	573	9110	9110	1134	0.008	1331	332.24	MOE Extended Detention	332.20
332.30	0.30	5918	586	9695	9695	1720	0.011				332.30
332.40	0.40	6042	598	10293	10293	2318	0.013				332.40
332.50	0.50	6167	610	10904	10904	2928	0.014				332.50
332.60	0.60	6293	623	11527	11527	3551	0.016	4062	332.69	25mm Event	332.60
332.70	0.70	6421	636	12162	12162	4187	0.017	4682	332.78	1:2 Year Event	332.70
332.80	0.80	6631	653	12815	12815	4840	0.079				332.80
332.90	0.90	6730	668	13483	13483	5508	0.192	5961	332.97	1:5 Year Event	332.90
333.00	1.00	6831	678	14161	14161	6186	0.336	6617	333.07	1:10 Year Event	333.00
333.10	1.10	6933	688	14849	14849	6874	0.508	7494	333.20	1:25 Year Event	333.10
333.20	1.20	7036	698	15548	15548	7572	0.702	8138	333.29	1:50 Year Event	333.20
333.30	1.30	7139	709	16256	16256	8281	0.916	8845	333.38	1:100 Year Event	333.30
333.40	1.40	7244	719	16976	16976	9000	1.149				333.40
333.50	1.50	7350	730	17705	17705	9730	1.399				333.50